
22.251 LAB Exercise 1

CASMO-4 Pin Cell Calculations



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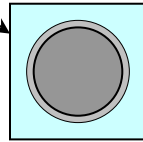
September 18, 2009

Core simulation sequence



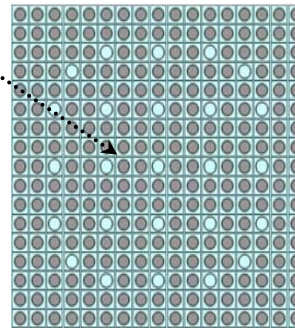
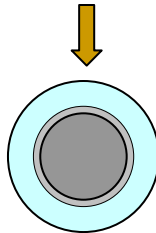
Basic data base:
cross-sections,
decay data

Multi-group
cross sections

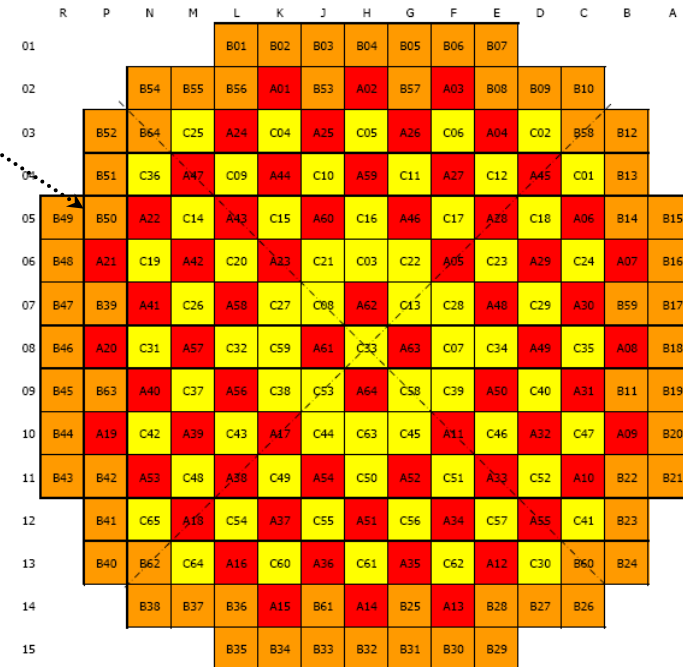


Unit cell

1D transport of
equivalent cell



Fuel assembly
2D transport or
diffusion



Reactor core
3D diffusion

- Get basic cross-sections
- Generate multi-group library
- Unit-cell Calculations
- Fuel Assembly/ Lattice Calculations
- Whole Core Calculations



LWR Core Simulations

- Lattice physics codes (e.g. CASMO) are used to prepare problem-dependent few group cross sections based on a smaller region (e.g. fuel assembly) for input to a whole-core program (e.g. SIMULATE).
- The CASMO few group cross sections are curve fitted to functions of important variables such as burnup, moderator temperature and void content, fuel temperature, soluble poison concentration ...
- These workhorse codes (CASMO) are all deterministic. There is also growing use of stochastic “Monte Carlo” programs for these applications (MCNP will be introduced in later lab sessions), but code running times are still excessive for many purposes.

Computer codes

- Transport-burnup codes
 - Infinite lattice, fuel cell or assembly
 - Many energy groups
 - Region average cross-section data
 - Time (burnup) dependant
 - Operation condition dependent (Tf, Tm, Power, Xe, Boron conc.)
- Nodal Diffusion codes
 - 3D core power distribution
 - 2 energy groups
 - Account for thermal feedback

Reactor Theory Uses

- Slowing down
 - Energy spectrum calculation
 - Homogenization of heterogeneous regions
- Transport
 - Spatial power distribution where diffusion does not work
 - Preparation of region averaged cross-sections
- Diffusion
 - Nodal methods for 3D core power distribution
- Burnup
 - Evolution of nuclide concentrations with time

Current Code Sets Used for LWR Reload Analysis

Code supplier	Code set*	Users		
		<u>Vendor</u>	<u>Licensee</u>	<u>Consultant</u>
ABB-CE	PHOENIX/POLKA	✓	✓	
B&W/Framatome	CASMO**/NEMO	✓	✓	
General Electric	TGEBLA/PANACEA	✓	✓	
Siemens	CASMO**/MICROBURN	✓	✓	
Westinghouse	PHOENIX/ANC	✓	✓	
EPRI	CPM-2/NODE-P		✓	✓
EPRI	CPM-2/SIMULATE-E		✓	✓
EPRI	CPM-3/CORETRAN			✓
Studsvik	CASMO**/SIMULATE-3**		✓	✓
Scanpower***	HELIOS/RAMONA		✓	

* Many different versions of these codes are in use today

** Codes developed by Studsvik of America

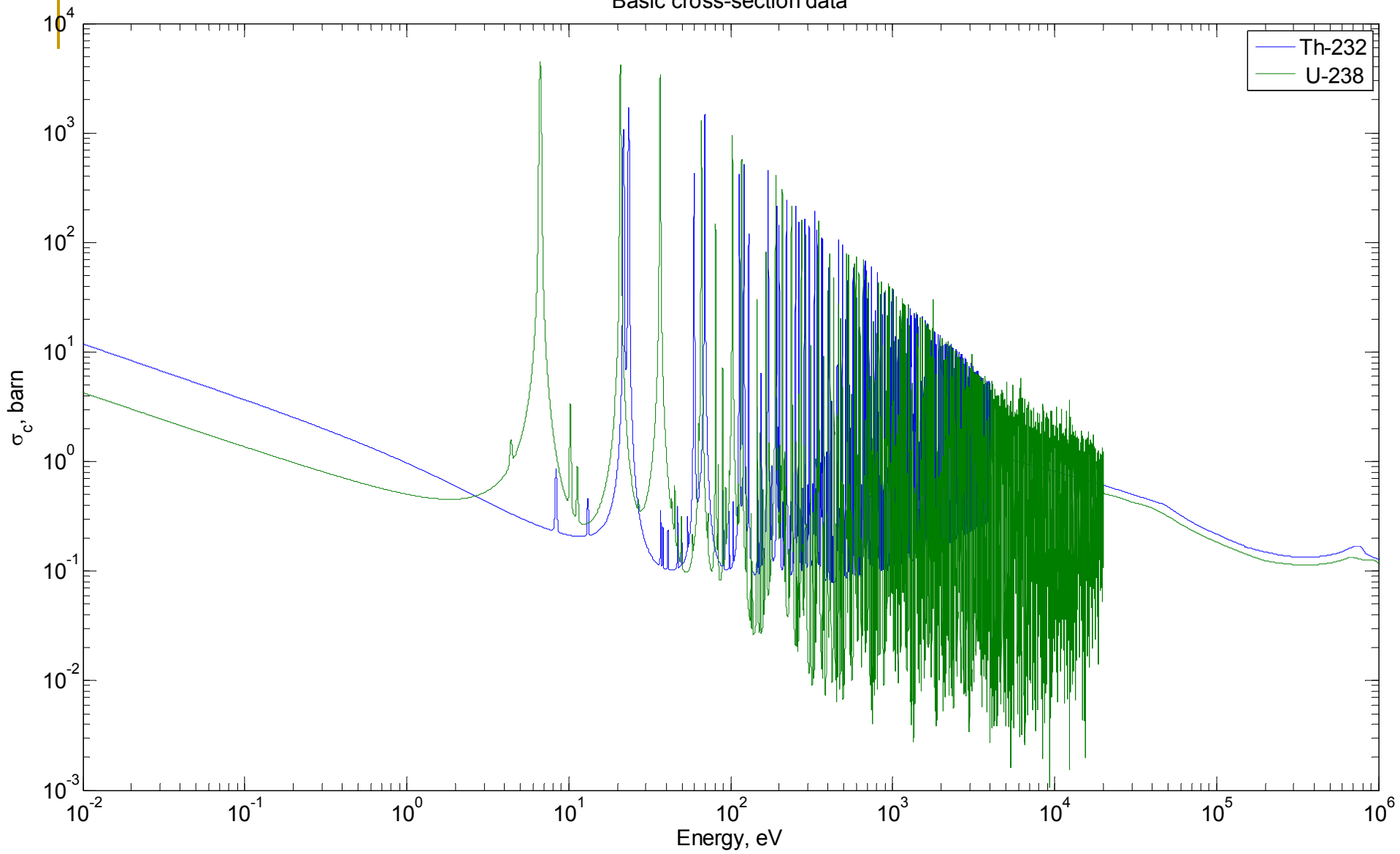
*** Scanpower has merged with Studsvik



Basic data libraries

- Core simulation requires nuclear data for all isotopes relevant to nuclear reactor design
 - Actinides, fission products, structural and control materials.
- Basic data includes:
 - Decay data: decay constants, decay modes, branching ratios, etc
 - XS for neutron reactions: (n, n) , (n, n') , $(n, 2n)$, (n, c) , (n, f) , etc
- Basic XS data libraries:
 - Contain microscopic XS data,
 - Cover wide neutron energy range (0 – 15 MeV).
 - Include thousands of energy points and interpolation schemes.
 - Resonance XS treated by special mathematical models.
 - Most use ENDF-6 format
 - Examples:
 - Evaluated Nuclear Data Files (ENDF) – Latest: ENDF VII
 - Joint European Data Files (JEFF) – Latest: JEFF-3.1
 - The data is collected from a large amount of experimentally measured points, analyzed, and evaluated with additional theoretical models.
 - The libraries are available in public domain

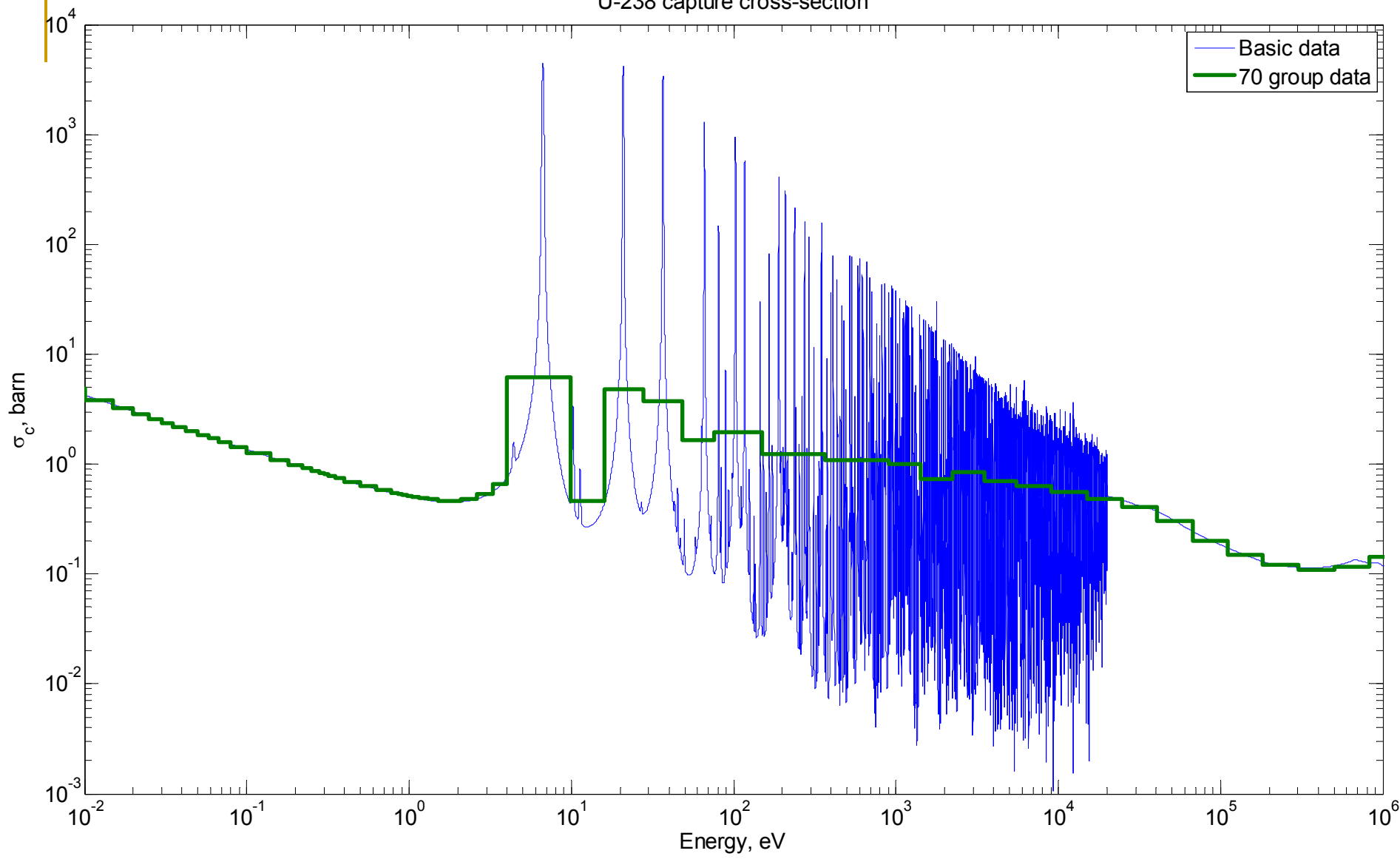
Basic cross-section data



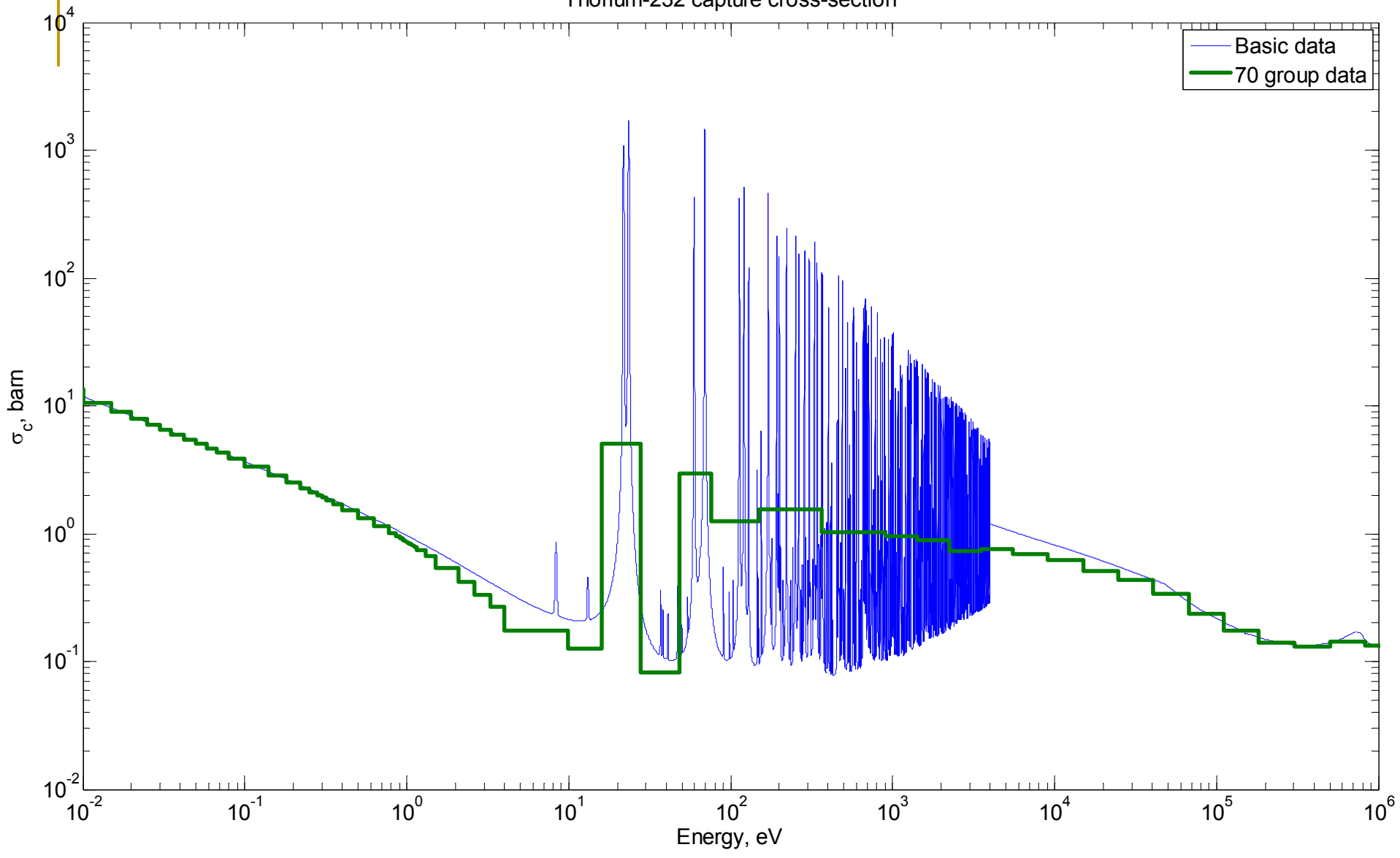
Multi-group XS library

- Routine reactor calculations:
 - Do not use directly the basic data libraries
 - Based on pre-processed multi-group (MG) libraries of microscopic XS
- MG library
 - Extends over the energy range of **0.001 eV – 10 MeV**
 - The range is divided into **~ 100 energy groups**
 - Each cross section comes with **one value for each group**
- MG XS must:
 - Conserve the **reaction rates**
 - Be tabulated as function of temperature
 - Include special scattering laws for moderators – $S(\alpha, \beta)$

U-238 capture cross-section

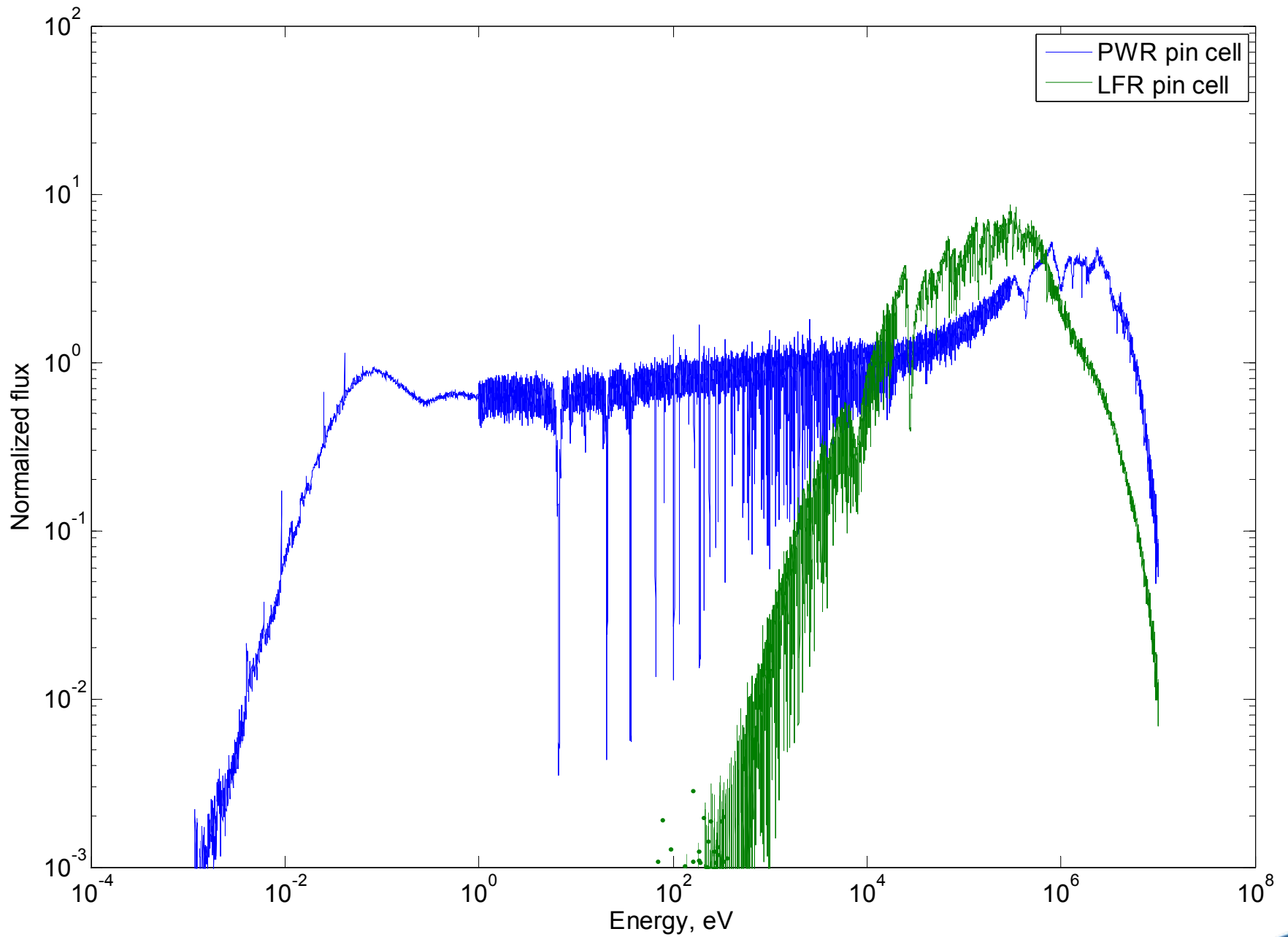


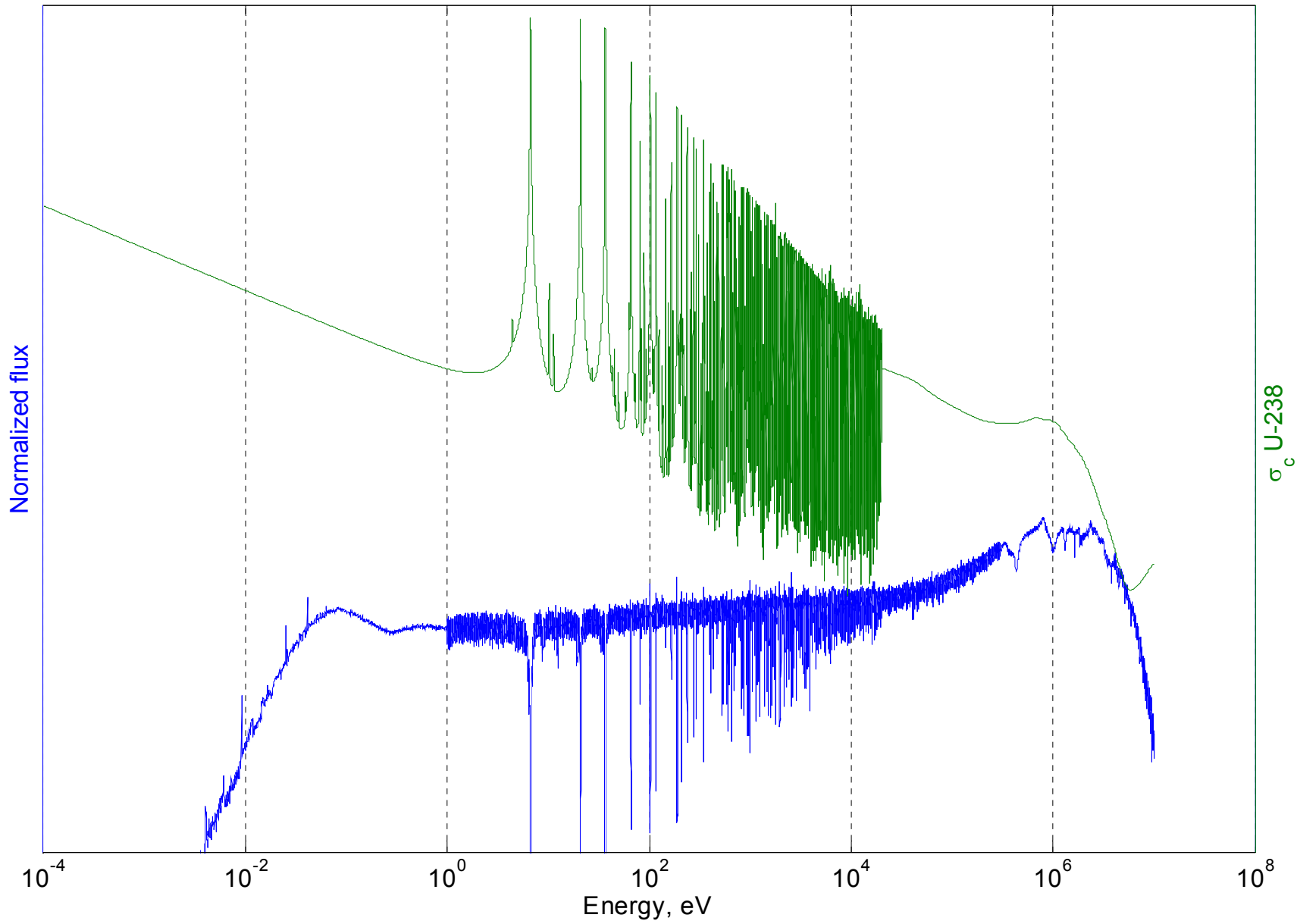
Thorium-232 capture cross-section

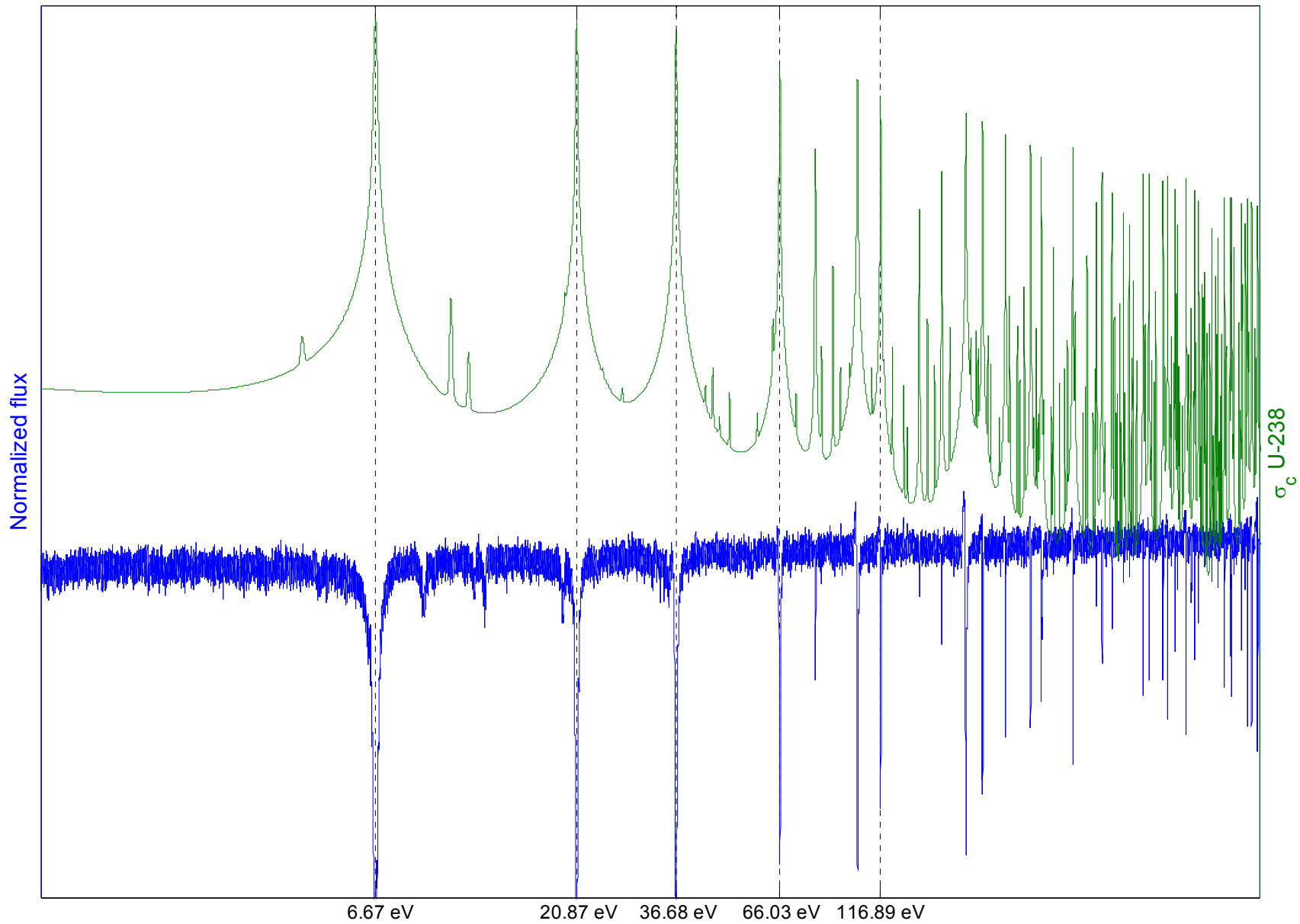


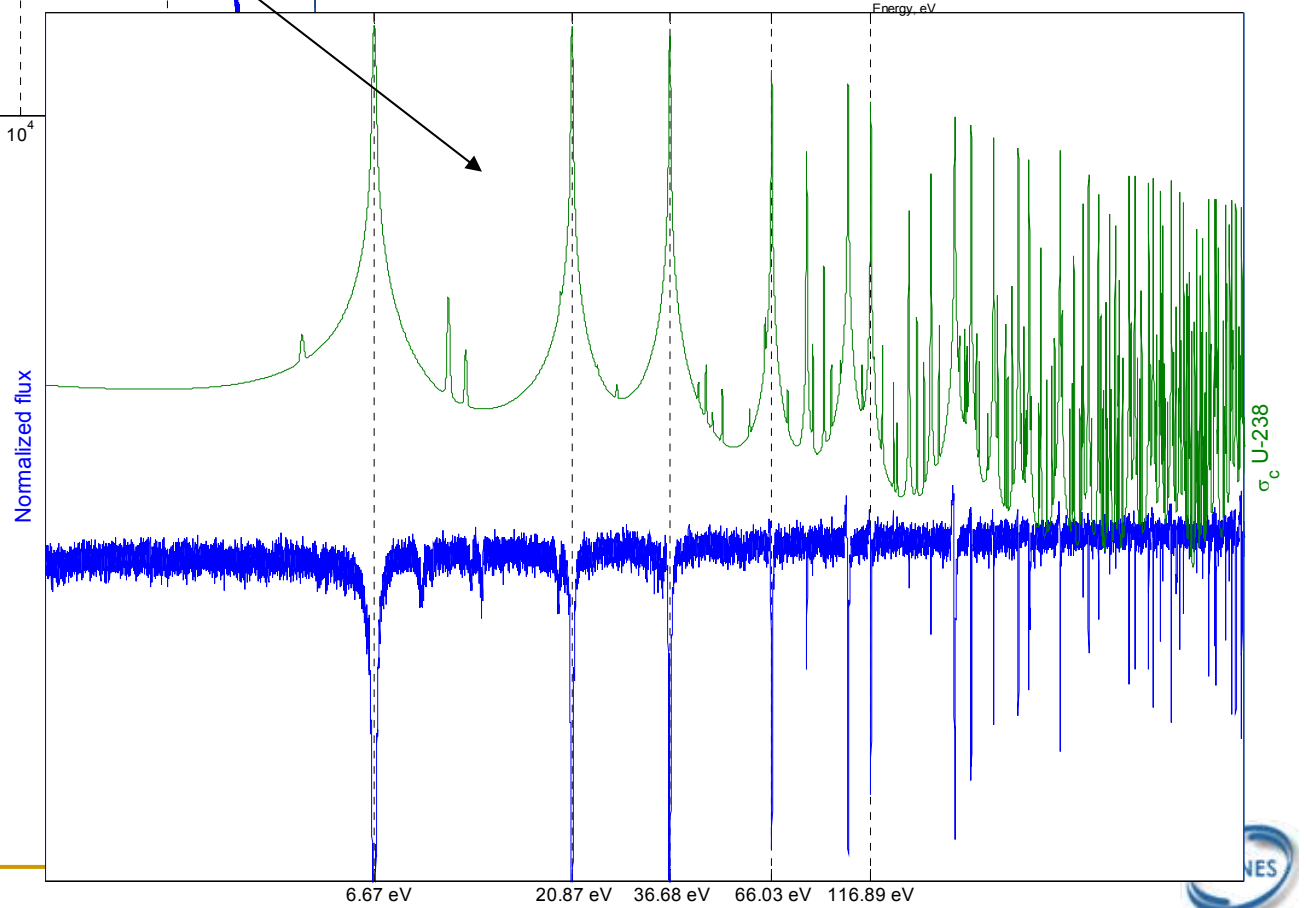
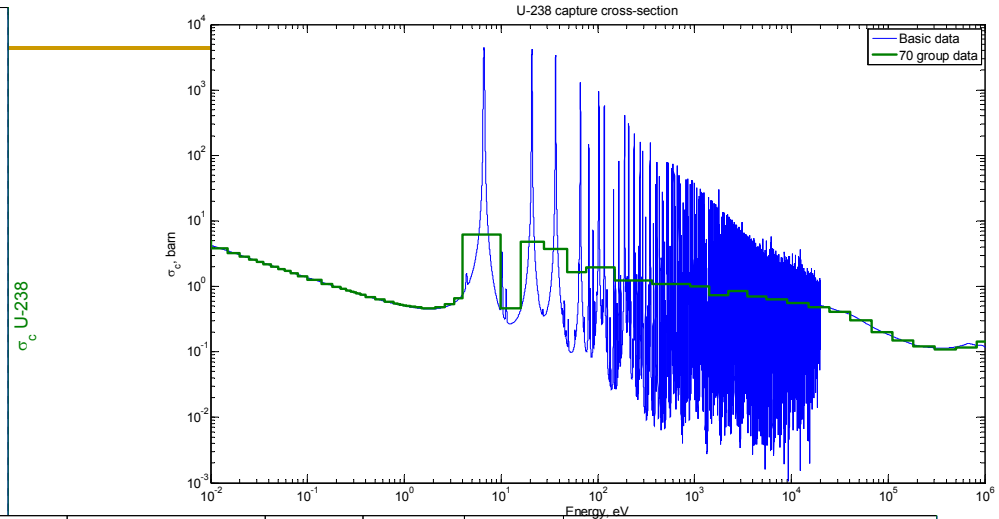
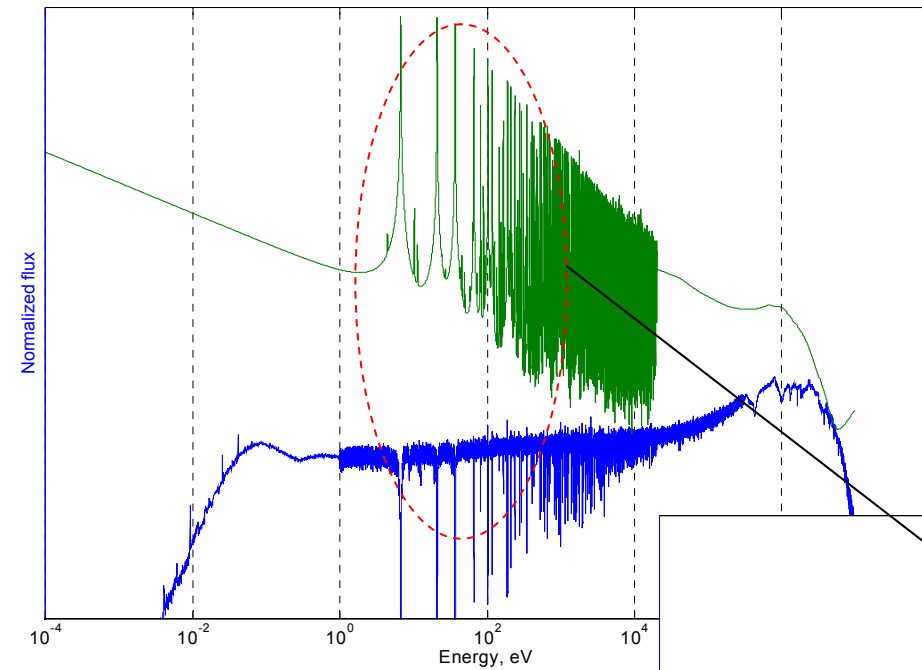
Unit cell calculations

- Unit-cell calculation precede those of the lattice
 - Basic assumption:
 - The fuel is arranged in an infinite lattice of identical cells
 - This results in zero currents on the cell boundaries
 - Never the case in reality
 - Example: PWR assembly – 264 fuel rods, 25 guide tubes
- but**
- Unit cell approach will suffice in obtaining the main physics characteristics of an average fuel rod.









Fuel depletion

- The rate at which the amount of nuclide N changes as function of time is given by a system of linear, homogeneous, first-order differential equations with constant coefficients:

$$\left\{ \begin{array}{l} \frac{dN_1(t)}{dt} = -\lambda_1 N_1(t) - \phi \sigma_1 N_1(t) + \lambda_2 BR_{2 \rightarrow 1} N_2(t) + \dots \\ \qquad \qquad \qquad \lambda_n BR_{n \rightarrow 1} N_n(t) + \phi (\sigma_{2 \rightarrow 1} N_2(t) + \dots \sigma_{n \rightarrow 1} N_n(t)) \\ \frac{dN_2(t)}{dt} = -\lambda_2 N_2(t) - \phi \sigma_2 N_2(t) + \lambda_1 BR_{1 \rightarrow 2} N_1(t) + \dots \\ \qquad \qquad \qquad \lambda_n BR_{n \rightarrow 2} N_n(t) + \phi (\sigma_{2 \rightarrow 2} N_2(t) + \dots \sigma_{n \rightarrow 2} N_n(t)) \\ \vdots \\ \frac{dN_n(t)}{dt} = -\lambda_n N_n(t) - \phi \sigma_n N_n(t) + \lambda_1 BR_{1 \rightarrow n} N_1(t) + \dots \\ \qquad \qquad \qquad \lambda_{n-1} BR_{n-1 \rightarrow n} N_{n-1}(t) + \phi (\sigma_{1 \rightarrow n} N_1(t) + \dots \sigma_{n-1 \rightarrow n} N_{n-1}(t)) \end{array} \right.$$

**Nomenclature is on
the next slide**



Fuel depletion

$$\frac{dN_j(t)}{dt} = -\lambda_j N_j(t) - \phi \sigma_j N_1(t) + \sum_{k=1}^{k=n} \lambda_k \text{BR}_{k \rightarrow j} N_k(t) + \phi (\sigma_{k \rightarrow j} N_k(t))$$

$N_i(t)$	-	Atoms of nuclide i at time t ,
$\frac{dN_i(t)}{dt}$	-	Rate of amount change of nuclide i ,
n	-	Number of nuclides,
λ_i	-	Radioactive decay constant of nuclide i (sec^{-1})
$\text{BR}_{k \rightarrow j}$	-	Branching ratio per decay of nuclide j to nuclide i .
σ_i	-	Single group Absorption cross section of isotope i .
$\sigma_{i \rightarrow j}$	-	Single group cross section leading from isotope i to isotope j .
ϕ	-	Flux.

Fuel depletion

Rate of change
of nuclide **i**

Disappear due
to decay

Disappear due
to neutron
absorption

$$\frac{dN_j(t)}{dt} = -\lambda_j N_j(t) - \phi \sigma_j N_j(t) +$$

Buildup due to
decay of other
nuclides

Buildup due to
absorption in
other nuclides

$$+ \sum_{k=1}^{k=n} \lambda_k \text{BR}_{k \rightarrow j} N_k(t) + \phi \left(\sum_{k=1}^{k=n} \sigma_{k \rightarrow j} N_k(t) \right)$$

Introduction to CASMO-4

- 2D, multi-group, neutron transport code for simulation of BWR/PWR assemblies or pin cells
- Uses metric units
 - densities in g/cm^3 , temperatures in Kelvin, dimensions in cm, burnup in MWd/kgIHM
- Automatic thermal expansion of dimensions and densities
- Input file is the problem description and consists of different *cards* (three character identifier). Default values are recommended.
- Comments begin with an asterisk (*)

Computer Running Information

- CASMO-4 is located in UNIX machine:
- Class account is 251 (username: 251, password: xxx)
- Use ssh for remote access, on athena* e.g.,
- After login, create your own directory, e.g., `mkdir xxx`
- Running command for CASMO-4 is `cas4`. Suppose your input file is `a. i np`, the running command would be

```
cas4 -J a. i np
```

Important note: include option `-J` to use JEF-2.2 library

Three files will be generated upon successful completion:

`a. l og` (log file), `a. out` (output), `a. cax` (card image)

- For a complete reference of how to use `cas4`, type

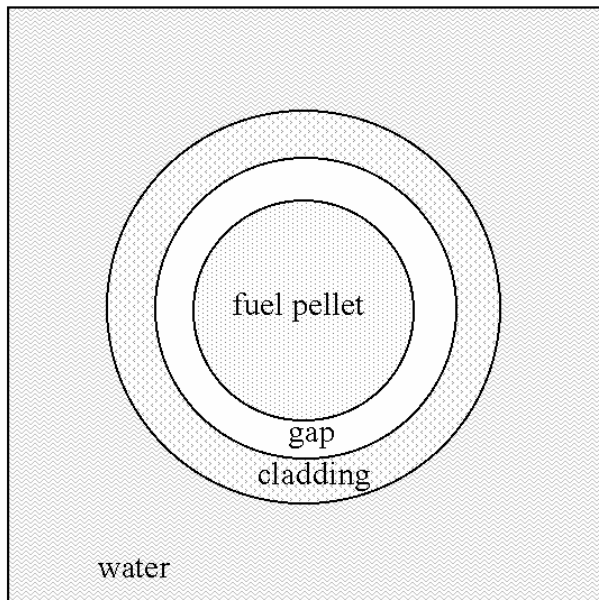
```
cas4 -h
```

*Athena is MIT's UNIX-based computing environment. OCW does not provide access to it.



Sample PWR unit cell input (2528.inp)

```
TTL * U235/U238, PWR PIN CELL
TFU=900 TMO=583.1
FUE 1 /1.16321E21 92234=0.0 92238=2.18219E22 8000=4.59686E22
PIN 1 0.4096 0.4178 0.4750/' 1' 'AIR' 'CAN'
PWR 2 1.26
PDE 104.5 'KWL'
DEP -80
STA
END
```



UO₂ fuel with 5 w/o U-235 (in total U)

Sample output (only summary is shown)

** C A S M O - 4 SUMMARY **

U235/U238, PWR PIN CELL

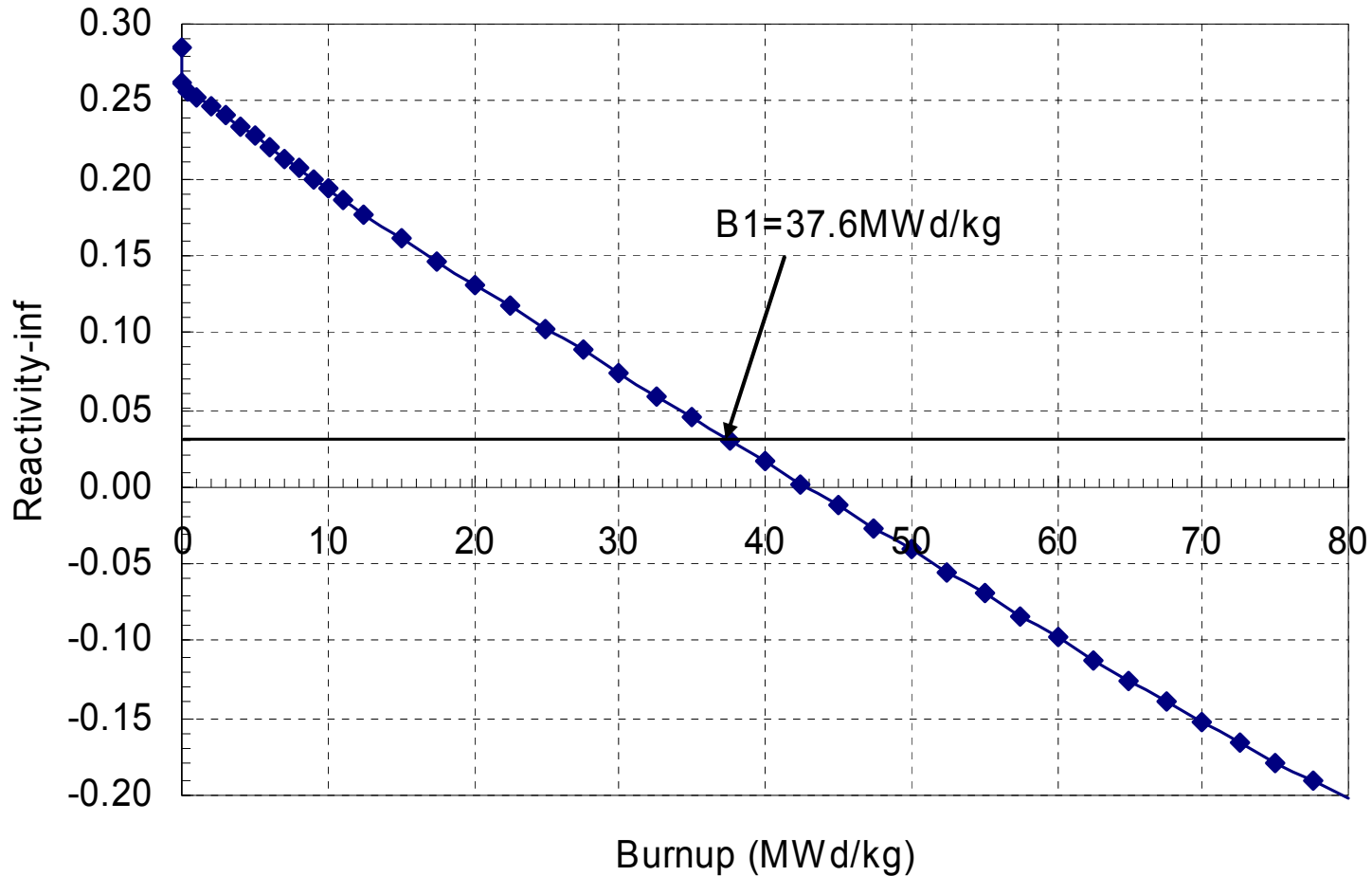
HVOI= 0.0 HTFU= 900.0 HTMO= 583.1 HTCO= 583.1 HBOR= 0.0

NO	VOID	TFU	TMO	TCO	BOR	ROD	BURNUP MWD/KG	K-INF	K-INF TWO-GROUP	M2	PIN PEAK	U-235 WT %	FISS PU WT %	TOT PU WT %
1	0.0	900.0	583.1	583.1	0.0		0.000	1.39812	1.39751	62.33	1.000	5.000	0.000	0.000
2							0.100	1.35589	1.35589	61.83	1.000	4.988	0.002	0.002
3							0.500	1.34620	1.34630	61.71	1.000	4.940	0.019	0.019
4							1.000	1.33867	1.33885	61.62	1.000	4.881	0.043	0.044
5							2.000	1.32742	1.32769	61.49	1.000	4.765	0.089	0.092
6							3.000	1.31627	1.31664	61.37	1.000	4.653	0.132	0.137
7							4.000	1.30493	1.30539	61.24	1.000	4.542	0.173	0.182
8							5.000	1.29355	1.29410	61.13	1.000	4.435	0.211	0.224
9							6.000	1.28228	1.28291	61.01	1.000	4.330	0.248	0.266
10							7.000	1.27122	1.27192	60.91	1.000	4.227	0.283	0.305
11							8.000	1.26041	1.26118	60.80	1.000	4.126	0.316	0.344
12							9.000	1.24990	1.25072	60.69	1.000	4.027	0.348	0.382
13							10.000	1.23969	1.24054	60.60	1.000	3.931	0.378	0.418
14							11.000	1.22976	1.23065	60.51	1.000	3.836	0.407	0.453
15							12.500	1.21544	1.21638	60.38	1.000	3.697	0.448	0.504
16							15.000	1.19293	1.19389	60.19	1.000	3.475	0.512	0.585
17							17.500	1.17161	1.17258	60.01	1.000	3.264	0.569	0.660
18							20.000	1.15145	1.15240	59.85	1.000	3.062	0.621	0.731
19							22.500	1.13242	1.13331	59.71	1.000	2.870	0.667	0.797
20							25.000	1.11418	1.11501	59.58	1.000	2.687	0.709	0.858
21							27.500	1.09662	1.09737	59.46	1.000	2.513	0.746	0.916
22							30.000	1.07965	1.08031	59.34	1.000	2.346	0.780	0.971
23							32.500	1.06322	1.06377	59.23	1.000	2.188	0.810	1.022
24							35.000	1.04737	1.04780	59.13	1.000	2.038	0.836	1.069
25							37.500	1.03182	1.03212	59.02	1.000	1.895	0.860	1.114
26							40.000	1.01674	1.01691	58.93	1.000	1.760	0.880	1.157
27							42.500	1.00211	1.00213	58.85	1.000	1.632	0.898	1.196
28							45.000	0.98789	0.98776	58.77	1.000	1.510	0.914	1.233
29							47.500	0.97399	0.97370	58.69	1.000	1.396	0.927	1.269
30							50.000	0.96045	0.95999	58.61	1.000	1.288	0.938	1.302
31							52.500	0.94732	0.94670	58.54	1.000	1.186	0.948	1.333



Reactivity versus burnup

reference case 5 w/o U235 in U235 + U238



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22.251 Systems Analysis of the Nuclear Fuel Cycle
Fall 2009

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