Toolbox: Electrical Systems Dynamics

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OUTLINE

- AC and DC power transmission
- Basic electric circuits
- Electricity and the grid

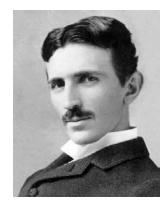
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"The war of the currents"

Pros and Cons

- One kills elephants
- One has simpler infrastructure
- Why do we have AC and not DC?
- Look at a simple transmission circuit to decide.
- Use Voltage=120 VDC and Power=1.2 GW



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Edison

EFFICIENT TRANSMISSION REQUIRES AC

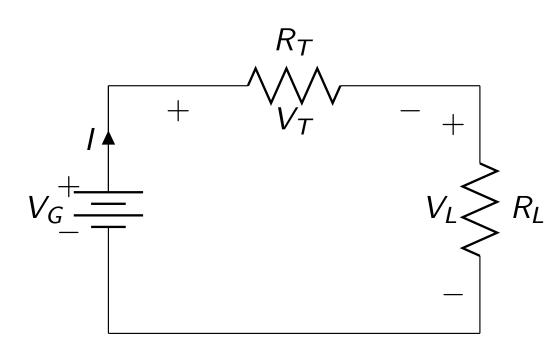
AC

□ Goals of the analysis

- Find the generator voltage
- Find the power delivered by the generator
- Find the power dissipated by the transmission line
- Find the ratio $P_{\text{Trans}}/P_{\text{Load}}$

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A SIMPLE ELECTRIC CIRCUIT



- **D** The current $I = \frac{V_L}{R_l}$
- □ The power to the load $P_L = I^2 R_L = \frac{V_L^2}{R_L}$
- □ Equating currents (from Kirchhoff's Laws), the transmission line power $P_T = I^2 R_T = \frac{R_T V_L^2}{R_L}$
- □ The power ratio is then the ratio of resistances: $\frac{P_T}{P_L} = \frac{R_T}{R_L}$
- □ Generator power

$$P_G = P_L + P_T = \left(1 + \frac{R_T}{R_L} \frac{V_L^2}{R_L}\right)$$

□ Generator voltage $V_G = \frac{P_G}{I} = 1 + \left(\frac{R_T}{R_L}\right) V_L$

Efficiency requires most power is dissipated in the load

AC

Example for Al and household V

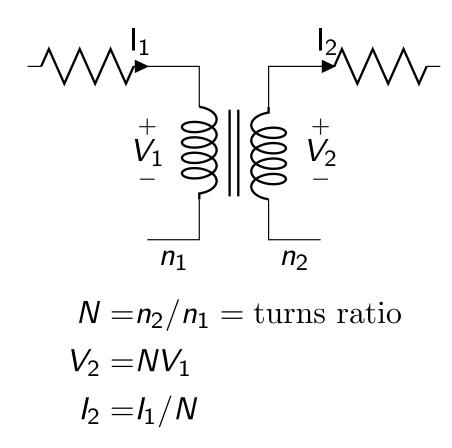
- □ If $R_T/R_L \ll 1$, then $P_T \ll P_L$
- Most of the voltage appears across the load.
- So, we have very small transmission losses.

- \square For $P_L = 1.2$ GW and $V_L = 120$ V
- $\square \text{ Then } R_L = P_L / V_L^2 = 1.2 \times 10^{-5} \Omega$
- For transmission assume L = 50 km (a short distance)
- An Aluminum cable with A = 5 cm² (to minimize sag, Cu not used.)
- \square Resistivity of Al, $\eta = 2.8 \times 10^{-8} \Omega\text{-m}$
- $\Box \therefore R_T = \eta L/A = 2.8\Omega \gg R_L$
- □ Conclusion: not so good!

AC CAN BE USED TO INCREASE THE VOLTAGE

- □ With AC we can use transformers
- □ Step up the voltage at the generator
- □ Transmit power at high voltage, low current
- □ Step down the voltage at the load
- □ Transmitting at low current should reduce transmission losses

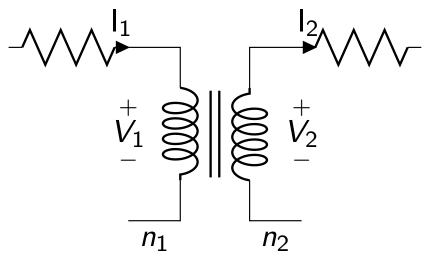
AN IDEAL TRANSFORMER



Physical process is conservation of magnetic flux/energy

AN IDEAL TRANSFORMER

Common examples of transformers:

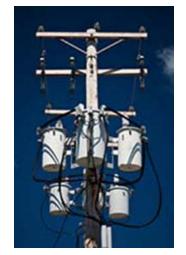


$$N = n_2/n_1 = \text{turns ratio}$$

 $V_2 = NV_1$
 $I_2 = I_1/N$

Physical process is conservation of magnetic flux/energy

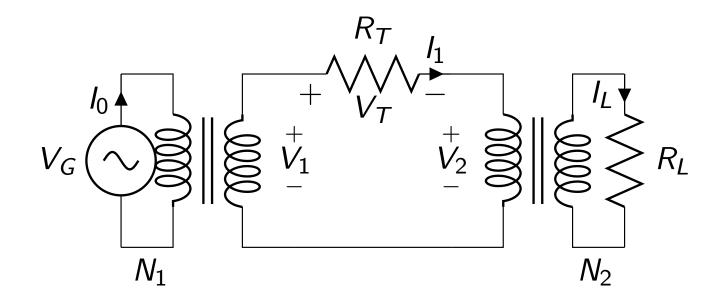






Bottom right: Photo by mdverde on Flickr. Bottom left: Image by Tau Zero on Flickr. Top right: Photo by brewbooks on Flickr.

AC TRANSMISSION REDUCES LOSSES



- \square As before, $P_L=1.2$ GW, $V_L=120$ V , $R_L=1.2\times 10^{-5}\Omega$
- □ What are transformer and transmission requirements,
- **□** Such that $P_T \ll P_L$?



From the circuit:

$$P_L = V_L I_L = R_L I_L^2$$
$$P_T = V_T I_1 = R_T I_1^2$$

□ From the transformer relation, $I_L = N_2 I_1$, it follows

$$\frac{P_T}{P_L} = \frac{1}{N_2^2} \frac{R_T}{R_L}$$



AC Analysis

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$$\frac{P_T}{P_L} = \frac{1}{N_2^2} \frac{R_T}{R_L}$$

□ For $N_2 \gg 1$ a huge reduction in transmission losses

Practical numbers:

$$V_0 = 12kV, V_1 = 240kV$$
 (rms)

- \square This implies that $N_1 = V_1/V_0 = 20$
- □ Assume small voltage drop across the transmission line. Then $V_2 \approx V_1$
- Second turn ratio becomes $N_2 = V_2/V_L = 2000$
- □ Our transmission loss formula gives $P_T/P_L \approx 6\%$

The downside to AC: Reactive power

- □ A down side to AC: Reactive power
- □ Why? Load is not pure resistive
- Load usually has an inductive component
- Resistance absorbs power
- □ Inductor circulates power back and forth
- □ This oscillating power is the reactive power

RESISTORS, INDUCTORS AND CAPACITORS, OH MY!

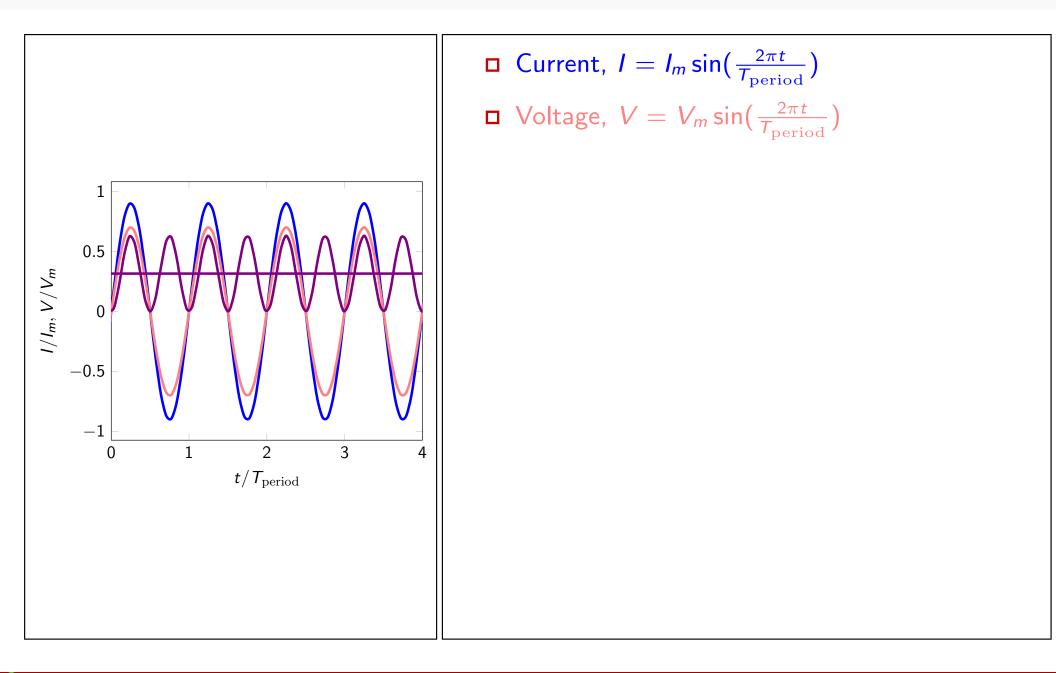
There are three basic circuit elements having different Ohm's laws.

Element	Resistor	Inductor	Capacitor
Symbol	R -	L -7000-	C
Ohm's Law	V = RI	$V = L \frac{dI}{dt}$	$\frac{dV}{dt} = I/C$
$I = \sin \omega t$	$V = R \sin \omega t$	$V = L \cos \omega t$	$V = -\frac{1}{C}\cos\omega t$
Phase shift	0	$\pi/2$	$-\pi/2$
Impedance $Z[\Omega] = V/I$	R	jωL	$\frac{-j}{\omega C}$

Reactive power

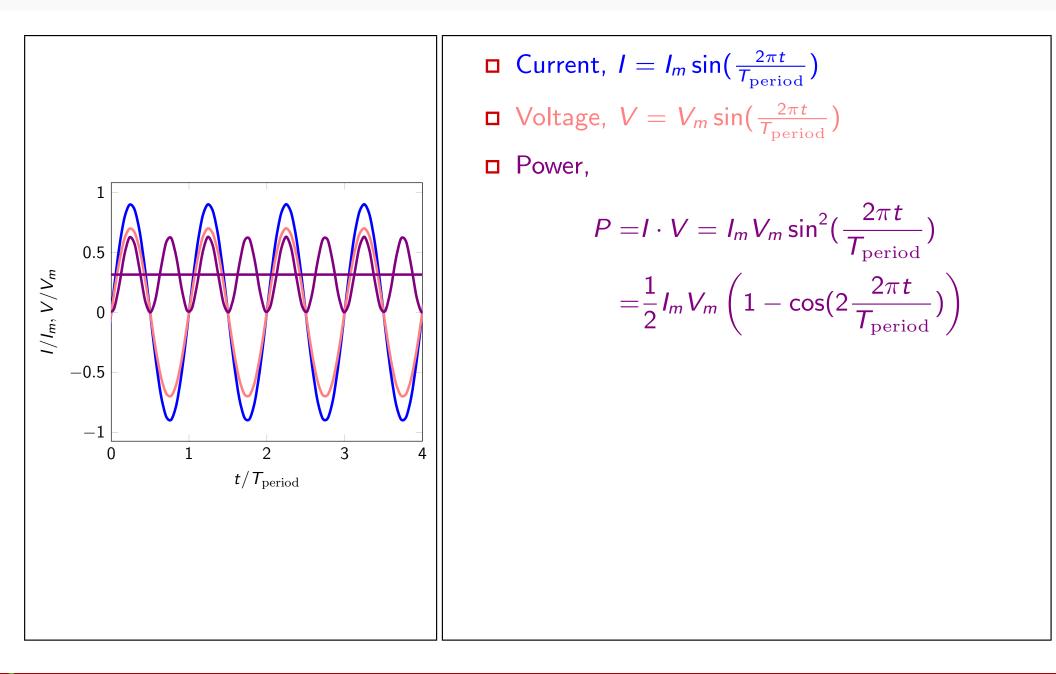
AC

PHASE LAGS INCREASE REACTIVE POWER



AC Reactive power

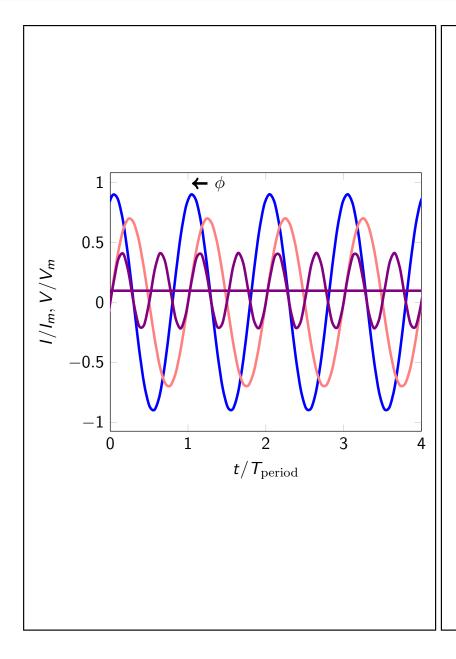
PHASE LAGS INCREASE REACTIVE POWER



Reactive power

AC

PHASE LAGS INCREASE REACTIVE POWER



 $\Box \text{ Current, } I = I_m \sin(\frac{2\pi t}{T_{\text{period}}} + \phi)$

• Voltage,
$$V = V_m \sin(\frac{2\pi t}{T_{\text{period}}})$$

□ Power,

$$P = I \cdot V = I_m V_m \sin\left(\frac{2\pi t}{T_{\text{period}}}\right) \sin\left(\frac{2\pi t}{T_{\text{period}}} + \phi\right)$$
$$= \frac{1}{2} I_m V_m \left(\cos(\phi) - \cos\left(2\frac{2\pi t}{T_{\text{period}}} + \phi\right)\right)$$

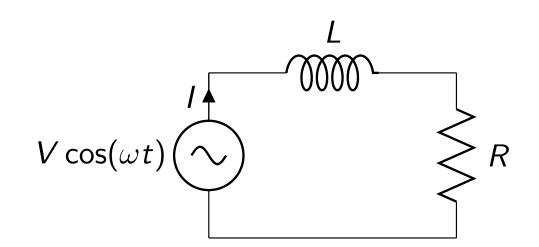
 $\cos(\phi)$ is known as the power factor

REACTIVE POWER MUST BE SUPPLIED.

- For parts of the AC cycle the instantaneous power is greater than the average power
- Generator must be able to deliver this higher power even though it is returned later
- Bottom line: generator must have a higher volt-amp rating than average power delivered: VARs and Watts.
- \square Higher rating \rightarrow bigger size \rightarrow higher cost

PHASE SHIFTS ARE INTRODUCED BY INDUCTANCE

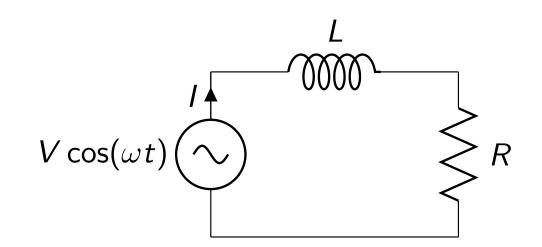
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□ It will introduce a phase shift given by $tan \phi = \frac{\omega L}{R}$

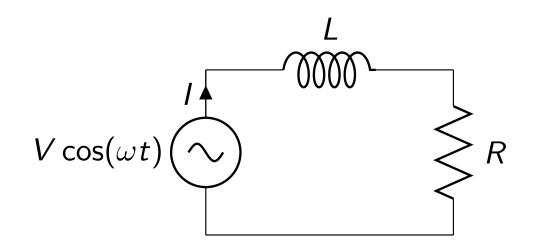


AC Reactive power

PHASE SHIFTS ARE INTRODUCED BY INDUCTANCE

- \square A motor will have an inductance, L.
- □ It will introduce a phase shift given by $tan \phi = \frac{\omega L}{R}$
- □ Amplitude of current will also be reduced.

$$I = \frac{V}{(\omega^2 L^2 + R^2)^{1/2}}$$



AC Reactive power

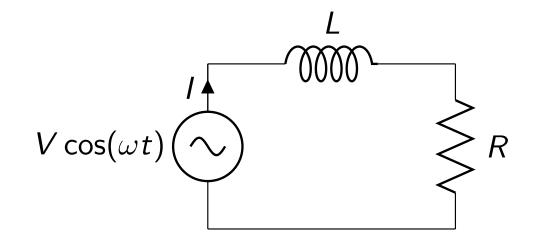
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□ This all follows from adding up the voltages for a simple circuit:

$$L\frac{dI}{dt} + RI = V\cos(\omega t)$$



How to minimize the VA requirement?

AC

- \square To minimize the VA requirements on the generator we want $\phi \rightarrow 0$
- \square Assume the average power absorbed by the load is $\langle P_L \rangle$
- \square Calculate the peak generator power $[P_G(t)]_{\max}$ as a function of $\langle P_L \rangle$
- **\square** Note: The peak is $2 \times$ (rms volt-amp rating)
- □ Less generator power is cheaper.

PEAK POWER FROM INDUCTANCE

□ The power dissipated in the load:

$$\langle P_L
angle = RI^2$$

 $= rac{RV^2}{\omega^2 L^2 + R^2}$

□ The peak power delivered by the generator

$$P_{\text{peak}} = VI \left(1 + \cos \phi \right) = \frac{V^2}{\left(\omega^2 L^2 + R^2 \right)^{1/2}} \left(1 + \frac{R}{\left(\omega^2 L^2 + R^2 \right)^{1/2}} \right)$$

 \square Using the expression for $\langle P_L \rangle$, we get:

$$\frac{P_{\text{peak}}}{2\langle P_L\rangle} = \frac{\left(\omega^2 L^2 + R^2\right)^{1/2} + R}{2R} \ge 1$$

CAPACITANCE CAN BALANCE OUT REACTIVE POWER

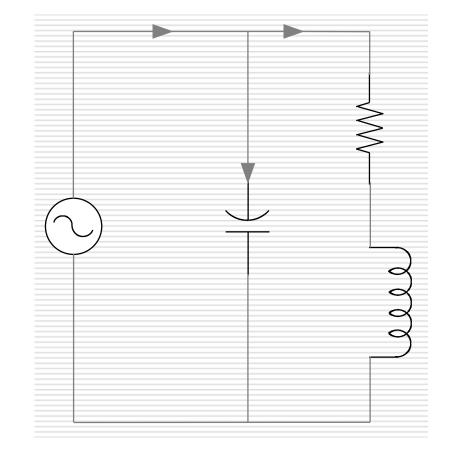
Recall from our table that the phase lags are opposite for inductance and capacitance

 \Box tan $\phi_L = \frac{\omega L}{R}$, tan $\phi_C = \frac{-1}{\omega C}$

Short answer: there is a capacitance that will keep the current and voltage in phase (but not eliminate the power factor)

$$C = \frac{L}{R^2 + \omega^2 L^2}$$

□ Long answer follows.



Analysis

I – V relation for a capacitor

$$\hat{I}_1(t) = C \frac{dV_G}{dt}$$

I – V relation for the load

$$V_{\scriptscriptstyle G} = R \hat{I}_2 + L \frac{d \hat{I}_2}{dt}$$

Conservation of current

$$\hat{I}(t) = \hat{I}_1(t) + \hat{I}_2(t)$$

Solution

- □ Assume $V_G = V \cos(\omega t)$ (all voltages now rms)
- Current in the capacitor branch

$$\hat{I}_1(t) = -\omega CV \sin(\omega t)$$

Current in the load branch (from before)

$$\hat{I}_2(t) = \frac{V}{\left(R^2 + \omega^2 L^2\right)^{1/2}} \cos(\omega t - \phi)$$

The total current

□ The total current flowing from the generator

$$\begin{split} \hat{I}(t) &= \hat{I}_1(t) + \hat{I}_2(t) \\ &= V \Biggl[\frac{\cos(\omega t - \phi)}{\left(R^2 + \omega^2 L^2\right)^{1/2}} - \omega C \sin(\omega t) \Biggr] \\ &= V \Biggl\{ \frac{\cos(\omega t) \cos \phi}{\left(R^2 + \omega^2 L^2\right)^{1/2}} + \Biggl[\frac{\sin \phi}{\left(R^2 + \omega^2 L^2\right)^{1/2}} - \omega C \Biggr] \sin(\omega t) \Biggr\} \end{split}$$

The value of C

- Choose C for zero reactive power
- Set sin(t) coefficient to zero

$$\omega C = \frac{\sin \phi}{\left(R^2 + \omega^2 L^2\right)^{1/2}}$$

Simplify by eliminating the power factor

$$C = \frac{L}{\left(R^2 + \omega^2 L^2\right)}$$

Calculate the peak power

Calculate the peak power to learn what has happened to the VA rating

$$egin{aligned} \mathcal{P}_{peak} &= \left[P_G(t)
ight]_{ ext{max}} = 2 \left[VI
ight]_{ ext{max}} \ &= 2 V^2 \, rac{\cos \phi}{(R^2 + \omega^2 L^2)^{1/2}} \ &= 2 rac{R \, V^2}{(R^2 + \omega^2 L^2)} \ &= 2 \left\langle P_L
ight
angle \end{aligned}$$

The Result

□ It worked!!

The VA requirement has been reduced

$$VA = \frac{P_{peak}}{2} = \left\langle P_L \right\rangle$$

DISCUSSION

- □ AC is good for transmission
- □ Have to manage reactive power

Other aspects:

- HVDC transmission lines
- □ AC losses from corona discharge
- Voltage and frequency tolerances
- Stability of the grid to perturbations, eg a power plant going offline or a transmission line going down.

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