## MIT Department of Mechanical Engineering 2.25 Advanced Fluid Mechanics

## Problem 4.04

This problem is from "Advanced Fluid Mechanics Problems" by A.H. Shapiro and A.A. Sonin


A nozzle with exit area $A_{2}$ is mounted at the end of a pipe of area $A_{1}$, as shown. The nozzle converges gradually, and we assum that the flow in it is (i) approximately uniform over any particular station $x$, (ii) incompressible, and (iii) inviscid. Gravitational effects are, furthermore, taken as negligible. The volume flow rate in the nozzle is given as $Q$ and the ambient pressure is $p_{a}$.
(a) Derive an expression for the gage pressure at a station where the area is $A(x)$.
(b) Show, by integrating the $x$-component of the pressure force on the nozzle's interior walls, that the net $x$-component of force on the nozzle due to the flow is independent of the specific nozzle contour and is given by

$$
F=\rho Q^{2} \frac{\left(A_{1}-A_{2}\right)^{2}}{2 A_{1} A_{2}{ }^{2}}
$$

(c) The expression in (b) predicts that F is in the positive $x$-direction regardless of whether the nozzle is converging $\left(A_{2}<A_{1}\right)$ or diverging $\left(A_{2}>A_{1}\right)$. Explain.

## Solution:

Given: $Q, A_{1}, A_{2}$ are constants.
(a) By mass conservation,

$$
(\text { mass in })=\rho v_{1} A_{1}=\rho v(x) A(x)=(\text { mass out })
$$

Since there is no change in the mass inside the CV:

$$
\begin{gathered}
v_{1} A_{1}=Q=v(x) A(x) \\
\Rightarrow v(x)=\frac{Q}{A(x)}
\end{gathered}
$$

Apply Bernoulli's equation along a stream line from station 1 to 2 :


Note that all the assumption required for Bernoulli have been satisfied:
(a) inviscid
(b) along a streamline
(c) steady
(d) constant density
(e) no work/energy input or loss

$$
\underbrace{p(x)+\frac{1}{2} \rho v(x)^{2}}_{\text {station 1 }}=\underbrace{p_{a}+\frac{1}{2} \rho v_{2}^{2}}_{\text {station } 2}
$$

Therefore,

$$
\begin{equation*}
p_{g}(x)=p(x)-p_{a}=\frac{1}{2} \rho\left(v_{2}^{2}-v^{2}\right) \quad \Rightarrow p_{g}(x)=\frac{1}{2} \rho Q^{2}\left(\frac{1}{A_{2}^{2}}-\frac{1}{A(x)^{2}}\right) \tag{4.04a}
\end{equation*}
$$

(b) Integrate the pressure along the nozzle to obtain the $x$-component of pressure force


$$
\begin{aligned}
F_{x}=\int_{1}^{2} d F_{x} & =\int_{1}^{2} p_{g}(x) d(\text { projected vertical area }) \\
& =\int_{A_{1}}^{A_{2}} p_{g} d\left(A_{1}-A\right)=-\int_{A_{1}}^{A_{2}} p_{g} d A
\end{aligned}
$$

We can reverse the integration limits to get rid of the minus sign in front and substitute Eq. (4.04a):

$$
\begin{align*}
F_{x} & =\int_{A_{2}}^{A_{1}} p_{g} d A \\
& =\rho Q^{2} \int_{A_{2}}^{A_{1}}\left(\frac{1}{A_{2}{ }^{2}}-\frac{1}{A^{2}}\right) d A \quad \Rightarrow F_{x}=\frac{\rho Q^{2}}{2} \frac{\left(A_{1}-A_{2}\right)^{2}}{A_{1} A_{2}{ }^{2}} \tag{4.04b}
\end{align*}
$$

(c)

For $\left(A_{2}<A_{1}\right), p_{g}(x)$ is positive. Since the pressure is greater on the inside than the outside, the net pressure force acts on the inner wall.

For $\left(A_{2}>A_{1}\right), p_{g}(x)$ is negative. Thus, the net pressure force acts on the outer wall, still pointing to the right.


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