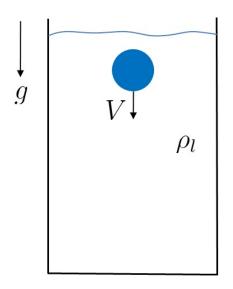
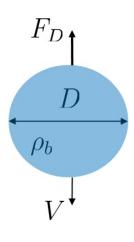
# MIT Department of Mechanical Engineering 2.25 Advanced Fluid Mechanics

#### Problem 7.03

This problem is from "Advanced Fluid Mechanics Problems" by A.H. Shapiro and A.A. Sonin

A metal ball falls at steady speed in a large tank containing a viscous liquid. The ball falls so slowly that it is known that the inertia forces may be ignored in the equation of motion compared with the viscous forces.





- (a) Perform a dimensional analysis of this problem, with the aim of relating the speed of fall V, to the diameter of the ball D, the mass density of the ball  $\rho_b$ , the mass density of the liquid  $\rho_l$ , and any other variables which play a role. Note that the "effective weight" of the ball is proportional to  $(\rho_b \rho_l)g$ .
- (b) Suppose that an iron ball (sp. gr.=7.9, D=0.3 cm) falls through a certain viscous liquid (sp. gr. = 1.5) at a certain steady-state speed. What would be the diameter of an aluminum ball (sp. gr. = 2.7) which would fall through the same liquid at the same speed assuming inertial forces are negligible in both flows?

#### **Solution:**

### (a) Non-dimensional Groups

In steady state, the body force (weight, W) must be balanced with buoyancy  $(F_B)$  and drag  $(F_D)$  forces.

$$W_{eff} = (\rho_b - \rho_l)g\left(\frac{4}{3}\pi \left(\frac{D}{2}\right)^3\right) = F_D \tag{7.03a}$$

Thus we have

$$n=5$$
 variables  $k=3$  primary variables  $\Rightarrow j=2$  dimensionless group

For our primary variables, we choose (1) a fluid property:  $\rho_l$ , (2) a flow parameter: V, and (3) a geometric parameter: D. Therefore, the first dimensionless group is

$$\mu = f_1(\rho_l, V, D)$$
 or  $\Pi_1 = K_1 \mu \rho_l^a V^b D^c$ 

where  $K_1$  is a constant. Thus,

$$M: 0 = 1 + a$$

$$L: 0 = -1 - 3a + b + c$$

$$T: 0 = -1 - b$$

$$\Rightarrow a = b = c = -1$$

$$\Pi_{1} = K_{1} \frac{\mu}{\rho_{l} V D} = \frac{K_{1}}{Re}$$
(7.03b)

Similarly, we can obtain the second non-dimensional parameter.

$$\Pi_2 = K_2 F_D \rho_l^a V^b D^c$$

$$\Rightarrow \boxed{\Pi_2 = K_2 \frac{F_D}{\rho_l V^2 D^2}}$$
(7.03c)

When  $K_2 = 2$ , this becomes the drag coefficient  $C_D$ , i.e.,

$$C_D = \frac{F_D}{\frac{1}{2}\rho V^2 A}$$

where A is a characteristic cross-section area.

#### (b) Example of Similarity

In part (a), we obtained two non-dimensional variables. In highly viscous flows or fast speed flows, the drag force is a function of the Reynolds number. However, if the speed of the ball is very small  $(Re \ll 1)$ , then the drag force is no longer a function of Reynolds number.

When the non-dimensional parameters are consistent in two situations, the flow fields are also similar. Let's make the drag coefficients are the same in the two cases.

$$C_D = \frac{(\rho_i - \rho_l)g\left(\frac{4}{3}\pi\left(\frac{D_i}{2}\right)^3\right)}{\rho V^2 D_i^2} = \frac{(\rho_a - \rho_l)g\left(\frac{4}{3}\pi\left(\frac{D_a}{2}\right)^3\right)}{\rho V^2 D_a^2}$$

where the subscripts i and a denote the iron and aluminum.

$$\Rightarrow \frac{(7.9 - 1.5) \times (0.3)^3}{(0.3)^2} = \frac{(2.7 - 1.5) \times D_a^3}{D_a^2}$$

Therefore, the diameter of an aluminum ball which satisfies the similarity is

$$\boxed{D_a = 1.6 \quad cm} \tag{7.03d}$$

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