

2.094

FINITE ELEMENT ANALYSIS OF SOLIDS AND FLUIDS

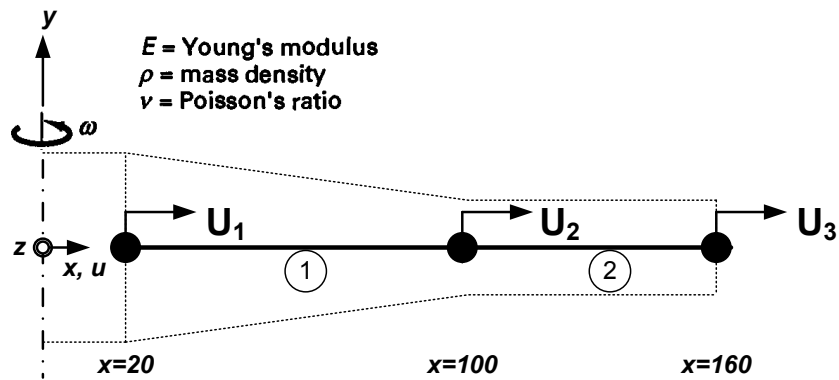
SPRING 2008

Homework 2 - Solution

Instructor: Prof. K. J. Bathe

Assigned: 02/14/2008
Due: 02/21/2008

Problem 1 (20 points):



In this problem, the global coordinate system is used.

Here, the non-zero strain components are $[\epsilon_{xx}, \epsilon_{zz}]$. Hence the stress-strain law represented by the matrix \underline{C} is

$$\underline{C} = \frac{E}{1-\nu^2} \begin{bmatrix} 1 & \nu \\ \nu & 1 \end{bmatrix}$$

And

$$\underline{\epsilon}^T = [\epsilon_{xx} \quad \epsilon_{zz}] = \begin{bmatrix} \frac{\partial u}{\partial x} & \frac{u}{x} \end{bmatrix}$$

$$\underline{U}^T = [U_1 \quad U_2 \quad U_3]$$

The applied force is given by

$$f_x^B(x) = \rho x \omega^2$$

The thickness of each element is given by

$$t^{(1)} = \frac{1}{80}(180 - x)$$

$$t^{(2)} = 1.0$$

For each element, the interpolation functions are

$$\underline{H}^{(1)} = \left[\frac{1}{80}(100 - x) \quad -\frac{1}{80}(20 - x) \quad 0 \right] \text{ for } 20 \leq x \leq 100$$

$$\underline{H}^{(2)} = \left[0 \quad \frac{1}{60}(160 - x) \quad -\frac{1}{60}(100 - x) \right] \text{ for } 100 \leq x \leq 160$$

Then,

$$\underline{B}^T = \left[\frac{\partial \underline{H}}{\partial x} \quad \underline{H} \right]$$

$$\underline{B}^{(1)} = \begin{bmatrix} -\frac{1}{80} & \frac{1}{80} & 0 \\ \frac{(100 - x)}{80x} & -\frac{(20 - x)}{80x} & 0 \end{bmatrix}$$

$$\underline{B}^{(2)} = \begin{bmatrix} 0 & -\frac{1}{60} & \frac{1}{60} \\ 0 & \frac{(160 - x)}{60x} & -\frac{(100 - x)}{60x} \end{bmatrix}$$

The stiffness matrices are

$$\begin{aligned} \underline{K} &= \int_{20}^{100} \underline{B}^{(1)T} \underline{C} \underline{B}^{(1)} dV^{(1)} + \int_{100}^{160} \underline{B}^{(2)T} \underline{C} \underline{B}^{(2)} dV^{(2)} \\ &= \int_{20}^{100} \underline{B}^{(1)T} \underline{C} \underline{B}^{(1)} t^{(1)} 2\pi x dx + \int_{100}^{160} \underline{B}^{(2)T} \underline{C} \underline{B}^{(2)} t^{(2)} 2\pi x dx \end{aligned}$$

The external force vector is

$$\begin{aligned} \underline{R} &= \int_{20}^{100} \underline{H}^{(1)T} \rho x \omega^2 dV^{(1)} + \int_{100}^{160} \underline{H}^{(2)T} \rho x \omega^2 dV^{(2)} \\ &= \int_{20}^{100} \underline{H}^{(1)T} \rho x \omega^2 t^{(1)} 2\pi x dx + \int_{100}^{160} \underline{H}^{(2)T} \rho x \omega^2 t^{(2)} 2\pi x dx \end{aligned}$$

Therefore we have

$$\underline{KU} = \underline{R}$$

After integrations using Matlab,

$$\underline{K} = \frac{E}{1 - \nu^2} \begin{bmatrix} 15.2590 - 10.4704\nu & -4.0988 + 1.0470\nu & 0 \\ -4.0988 + 1.0470\nu & 24.1192 + 2.0943\nu & -13.125 \\ 0 & -13.125 & 14.4885 + 6.2820\nu \end{bmatrix}$$

$$\underline{R} = \rho\omega^2 \begin{bmatrix} 944991 \\ 4521380 \\ 3732212 \end{bmatrix}$$

The same results are obtained using a local coordinate system for each element (like the example 4.5 in the textbook). For your reference, a sample solution using a local coordinate system is attached.

MIT OpenCourseWare
<http://ocw.mit.edu>

2.094 Finite Element Analysis of Solids and Fluids II
Spring 2011

For information about citing these materials or our Terms of Use, visit: <http://ocw.mit.edu/terms>.