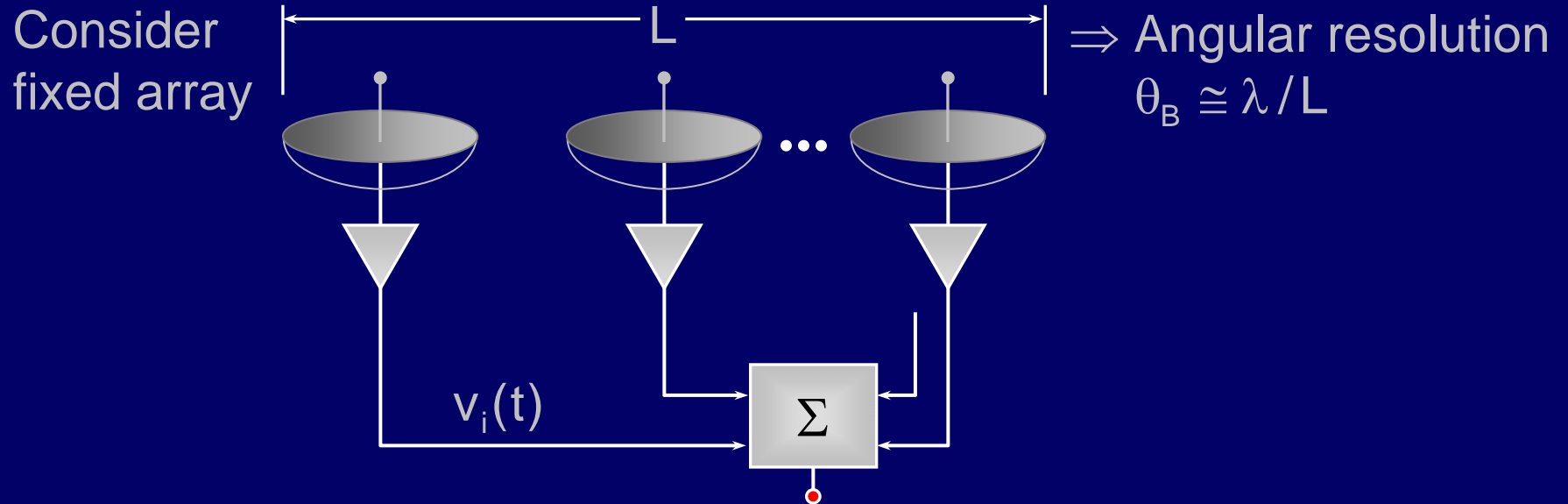


Synthetic Aperture Radar (SAR)

Basic Concept of SAR:

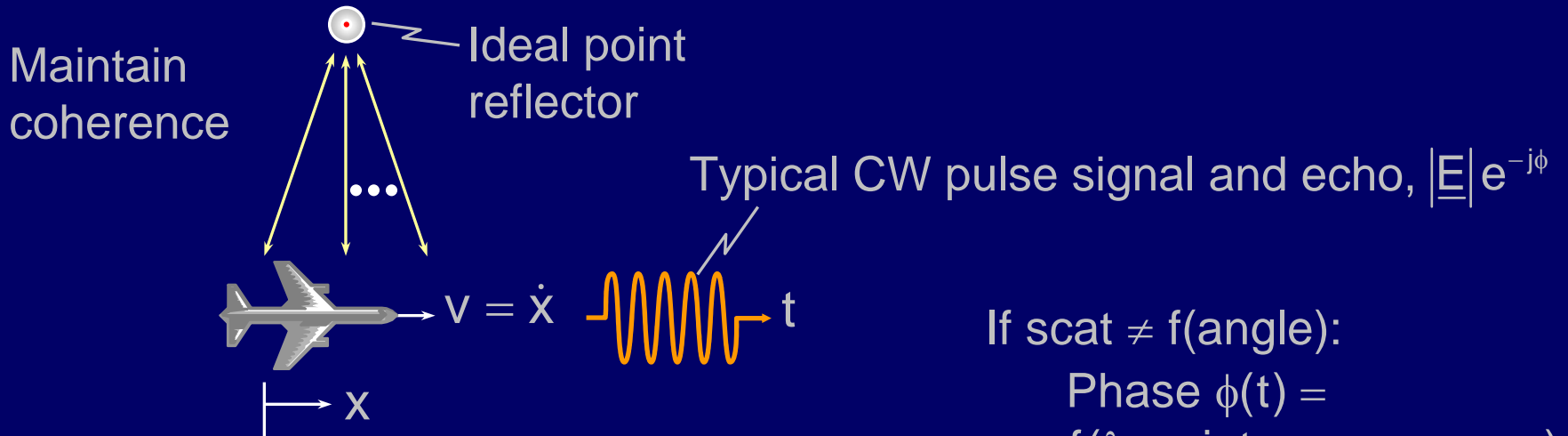


Claim Equivalent to Moving Antenna:

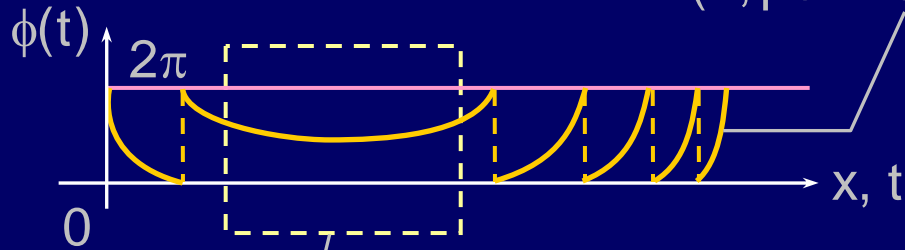
Assumes phase coherence in oscillator during each image



Synthetic Aperture Radar (SAR)

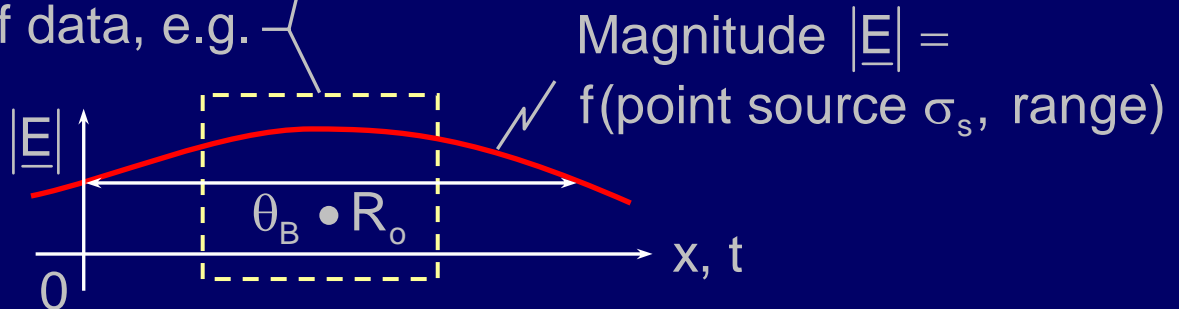


Received phase:



Process a "window" of data, e.g.

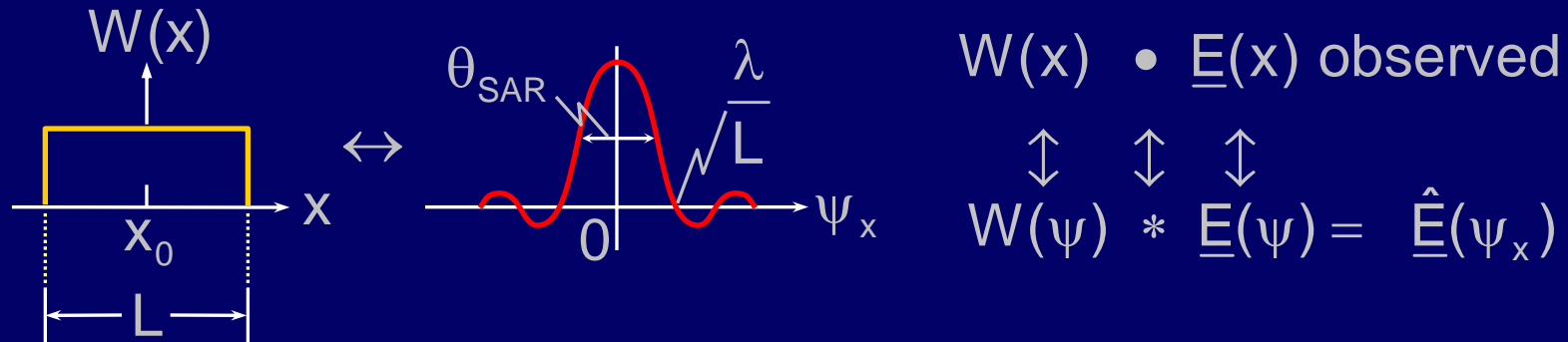
Received magnitude:



We seek 2-D source characterization: $\sigma_s = f(\text{azimuth, range})$

Resolution of "Unfocused" SAR

Reconstruction of image: first select R , x_0 of interest



SAR angular resolution: $\theta_{SAR} \cong \lambda/L_{SAR} \geq \lambda/R\theta_B = D/R$
 $\cong \lambda/D$

Resolution of "Unfocused" SAR

SAR angular resolution: $\theta_{\text{SAR}} \cong \lambda / L_{\text{SAR}} \geq \lambda / R \theta_B = D / R$
 $\cong \lambda / D$

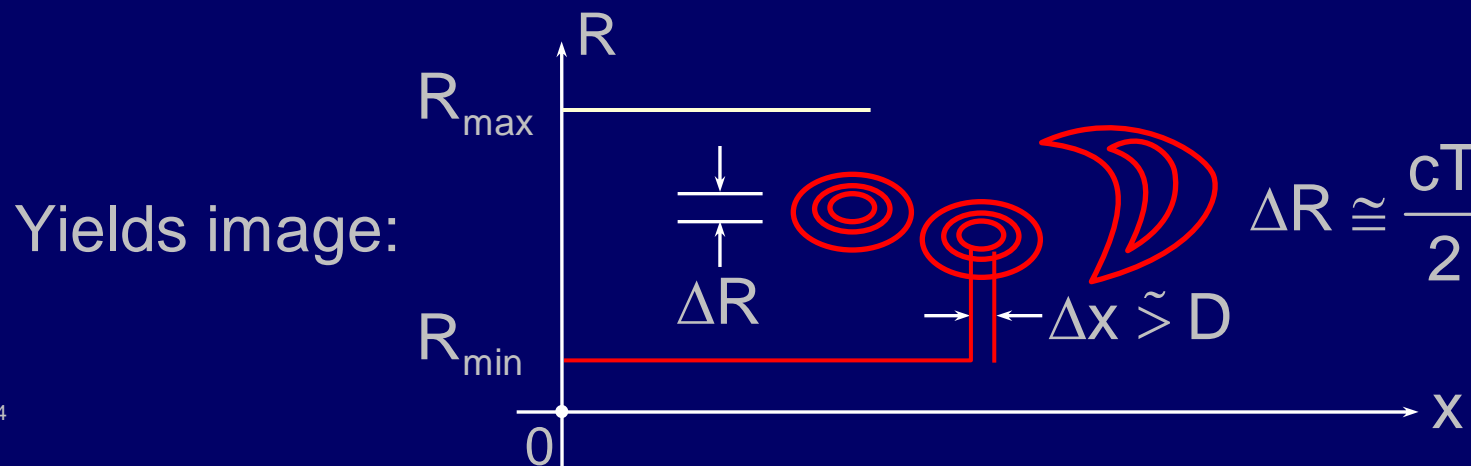
Lateral spatial resolution = $\theta_{\text{SAR}} \cdot R \cong D$

(want small D, large θ_B , large L)

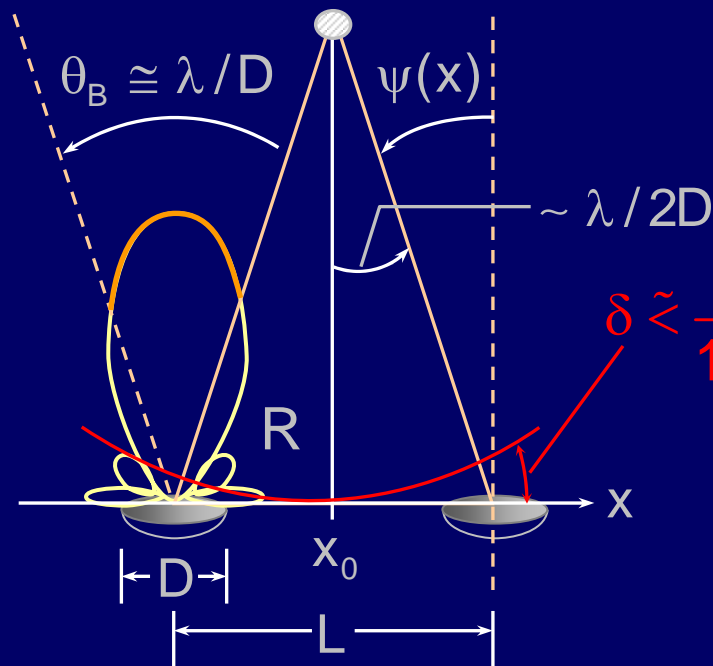
Range resolution $\cong cT / 2$

Note: If antenna is steered toward the target, increasing L, the lateral resolution can be $< D$.

Then repeat for all R, x_0



Phase-Focused SAR



$$\delta \lesssim \frac{\lambda}{16} \Rightarrow$$

$$R^2 + \left(\frac{L}{2}\right)^2 = (R + \delta)^2 \cong R^2 + 2\delta R$$

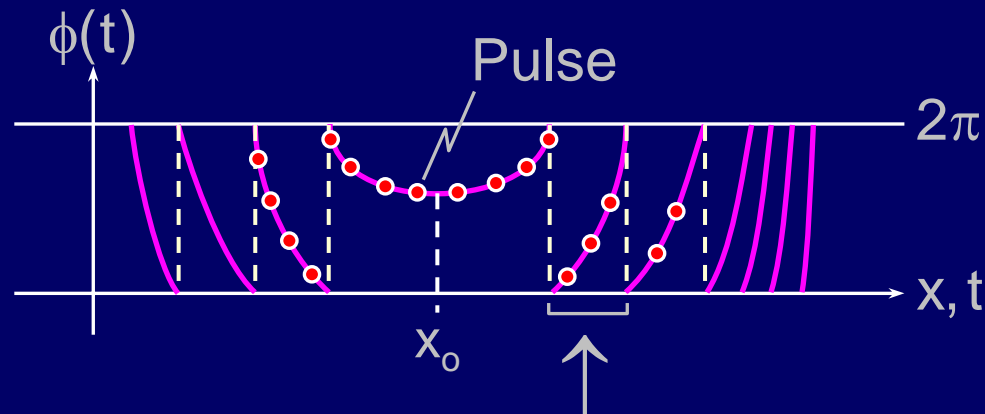
$$\delta \cong \frac{L^2}{8R} \leq \frac{\lambda}{16}$$

therefore $R \gtrsim \frac{2L^2}{\lambda}$ "farfield"
and focusing is unnecessary

Phase focusing is required if $\delta \gtrsim \lambda/16$,
so the target is in the SAR near field,
i.e., if $R \lesssim 2L^2 / \lambda = 2\lambda R^2 / D^2$ (where $L = \lambda / \theta_{\text{SAR}} = \lambda R / D$).

Phase-Focused SAR

Solution: $W(x) \rightarrow \underline{W}'(x)$ with phase correction

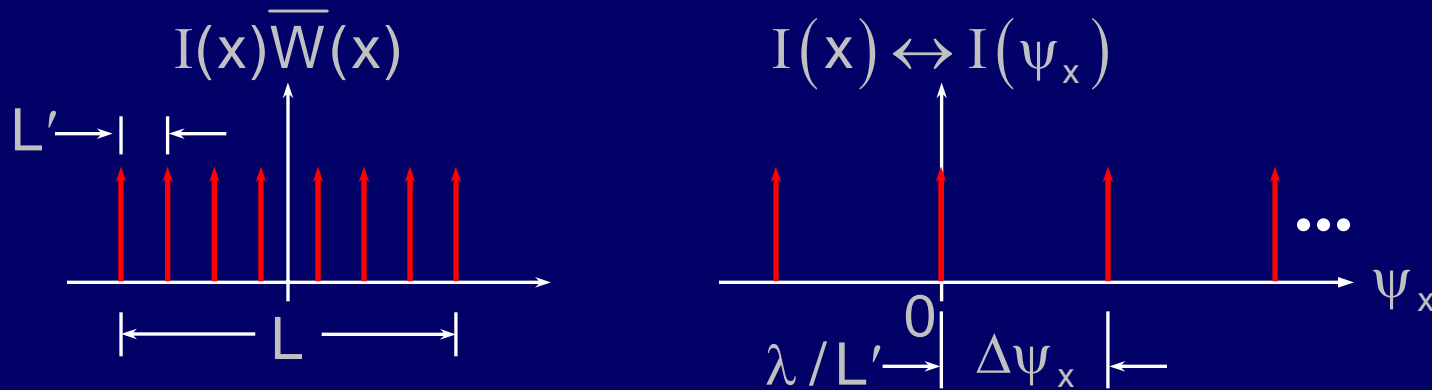


PRF must be higher; to reconstruct $\phi(t)$ we need at least 2 samples per phase wrap.

Note: With phase focusing, L increases and spatial resolution in x can be less than D , using beamsteering (e.g. a phased array)

Also: L.O. phase drift can be corrected if bright point sources exist in scene.

Required Pulse-Repetition Frequency (PRF)



$$W(x) \bullet I(x) \bullet \hat{\underline{E}}(x) \quad \text{Observed}$$

$$\updownarrow \quad \updownarrow \quad \updownarrow \quad \updownarrow \quad \updownarrow$$

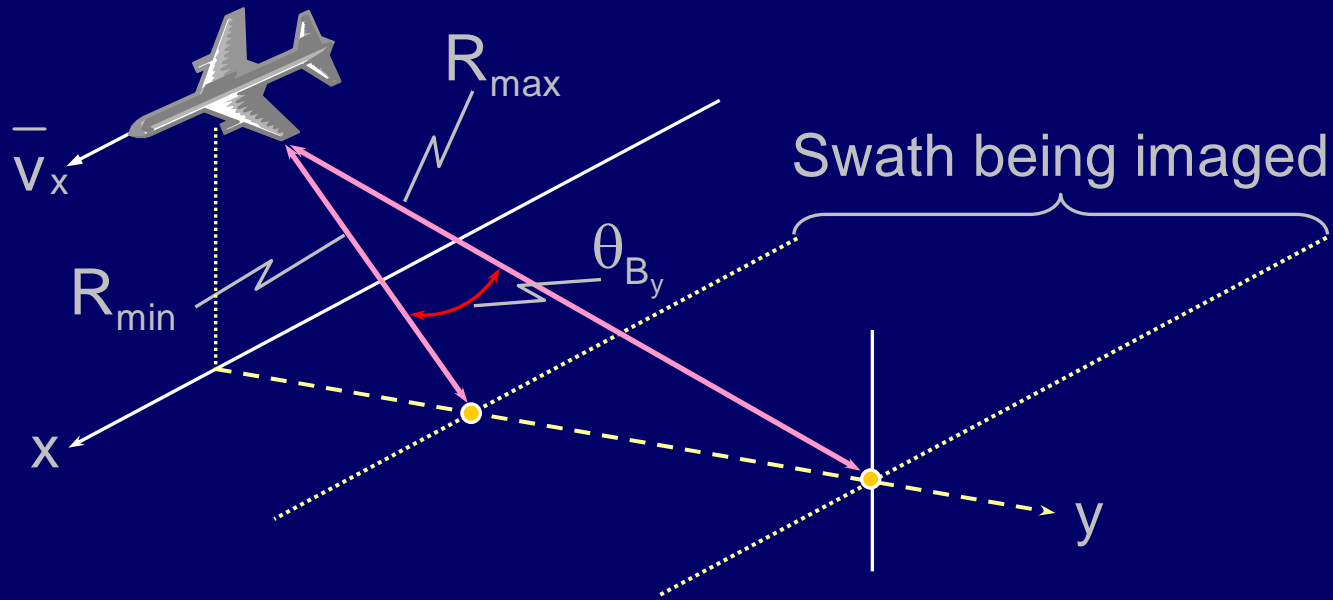
$$W(\psi_x) * I(\psi_x) * \underline{E}(\psi_x) = \hat{\underline{E}}(\psi_x)$$

PRF = v/L' (e.g., v = aircraft velocity)

Want $\Delta\psi_x = \lambda/L' \gg \lambda/D$, or $D \gg L'$

Therefore want PRF $\gg v/D$

PRF Impacts SAR Swath Width

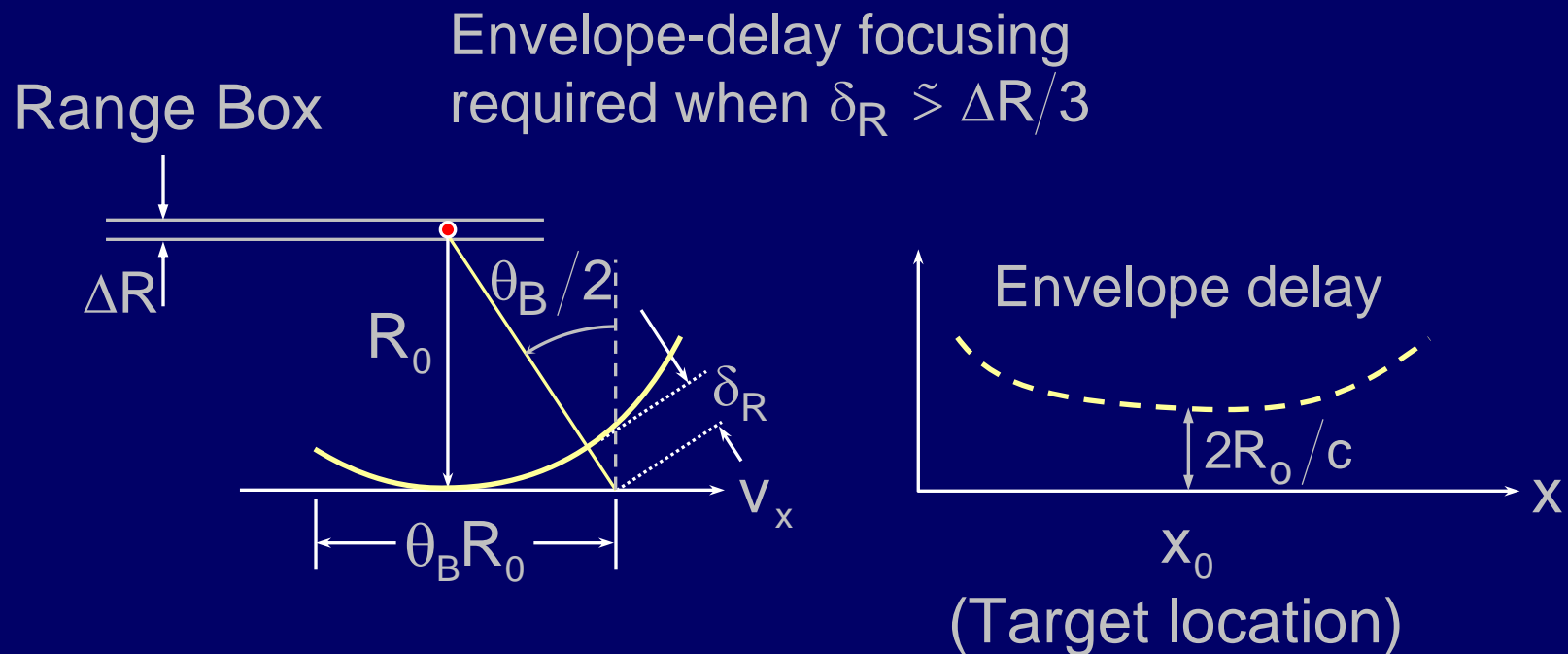


Don't want echoes to overlap for successive pulses.

$$\text{Therefore let } 2(R_{\max} - R_{\min})/c \lesssim \left(\frac{1}{\text{PRF}} \right) = L'/v_x \ll \frac{D}{v_x}$$

Implies that large swath widths require large $\frac{D}{v_x}$ and yield poorer spatial resolution.

Envelope Delay Focusing



Compensation for both envelope delay and phase delay is needed for very high spatial resolution [i.e., for small ΔR (large B)] and large $\theta_B R_0$.

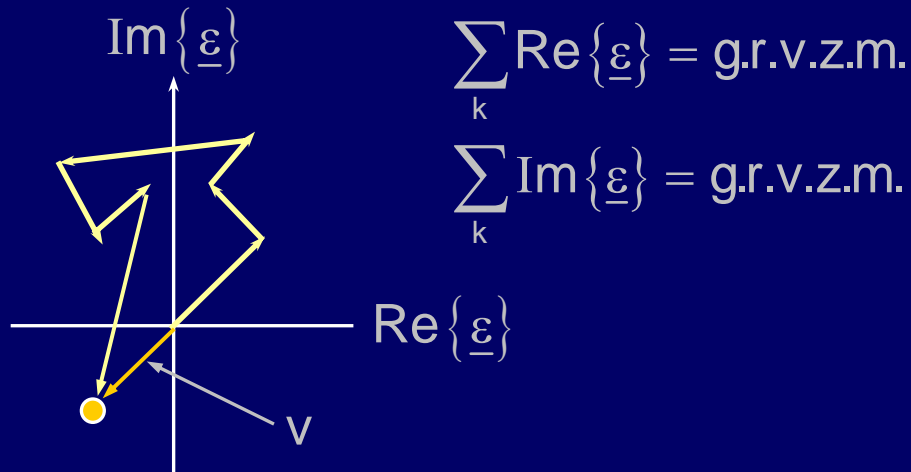
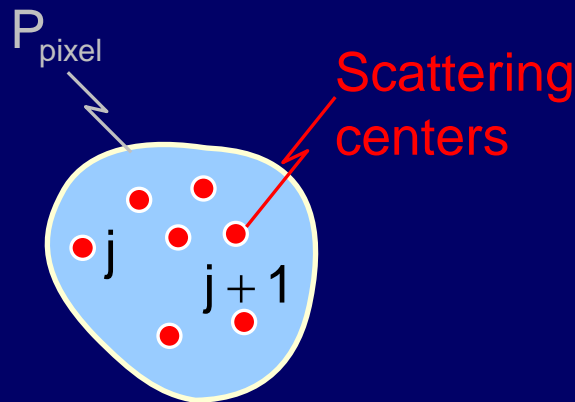
SAR Intensity Estimates: Speckle

For each SAR pixel, the estimated cross-section is:

$$\hat{\sigma} = K \left| \sum_{i,j} w(x_i) \underline{E}_{ij} \right|^2 \quad \text{where} \quad \begin{cases} K = \text{range-dependent constant} \\ i = \text{pulse number} \\ j = \text{subscattering index} \end{cases}$$

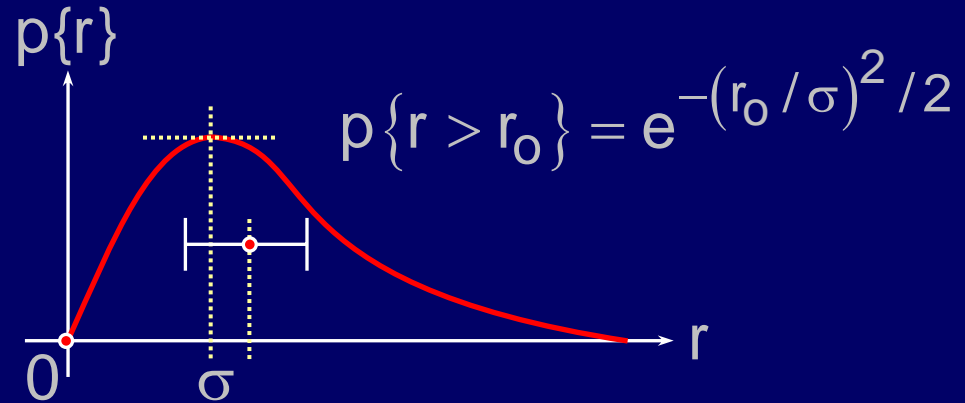
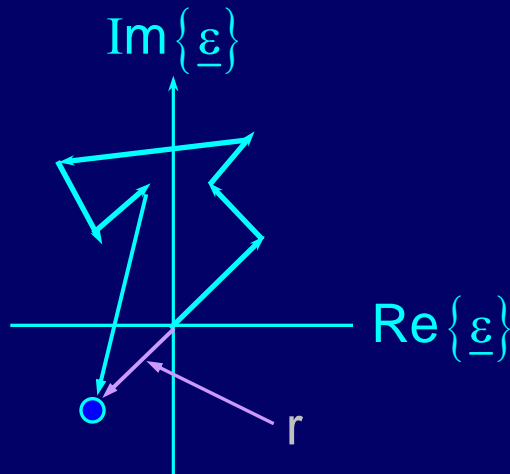
Many subscatters j per pixel

Simplifying:
$$\hat{\sigma} = \left| \sum_{k=1}^N \underline{\varepsilon}_k \right|^2 = \left| \sum_{k=1}^N \underbrace{a_k}_{\text{random variable}} e^{j(\omega t + \underbrace{\phi_k}_{\text{uniformly over } 2\pi \text{ typically}})} \right|^2 = |\underline{r}|^2$$



SAR Intensity Estimates: Speckle

$$p\left\{\underbrace{\left|\sum \underline{\varepsilon}_k\right|}_{\text{"r"}}\right\} = \frac{r}{\sigma^2} e^{-r^2/2\sigma^2}$$



$$E[r] = \sigma\sqrt{\pi/2}$$

$$E[r^2] = \sigma^2(2 - \pi/2) \propto |\underline{\varepsilon}|^2$$

Because we are adding (averaging) phasors, not scalars

$$\sqrt{E[r - \bar{r}]^2} \cong 2\sigma/3 \neq f(N)!$$

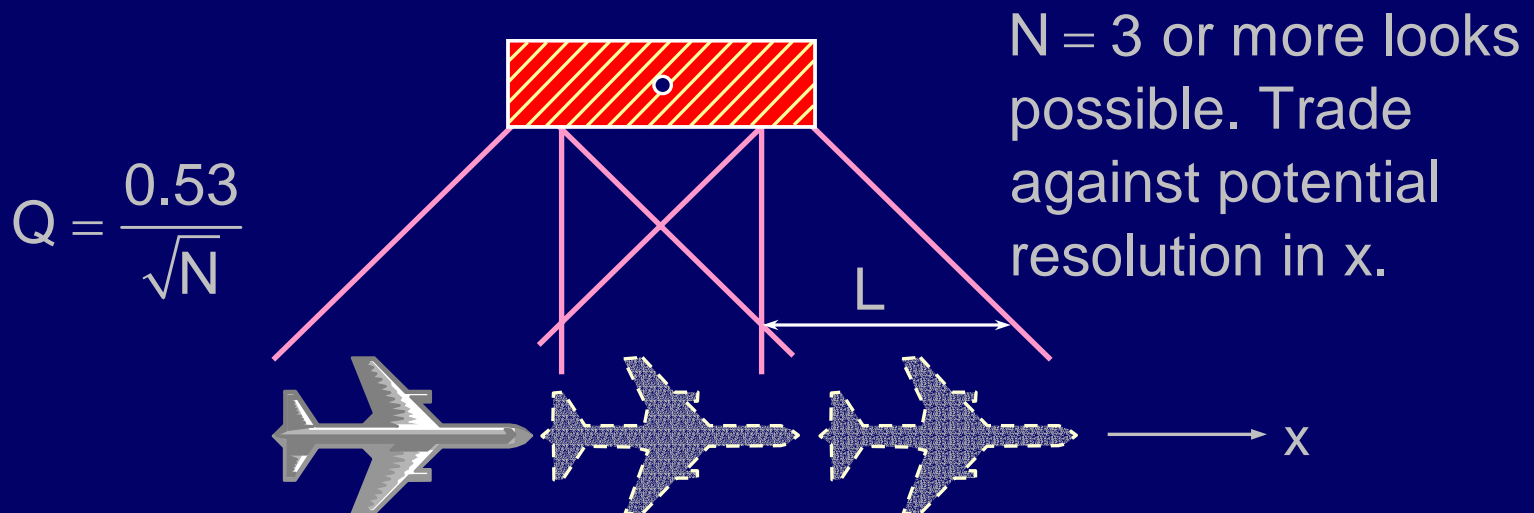
Thus raw SAR images, full spatial resolution,

have $\frac{\text{STD deviation}}{\text{mean intensity}} \triangleq Q \cong \frac{2\sigma/3}{\sigma\sqrt{\pi/2}} = 0.53 \Rightarrow \text{very grainy images}$

Reduction of SAR Speckle

Alternate ways to reduce "speckle" by averaging pixel intensities:

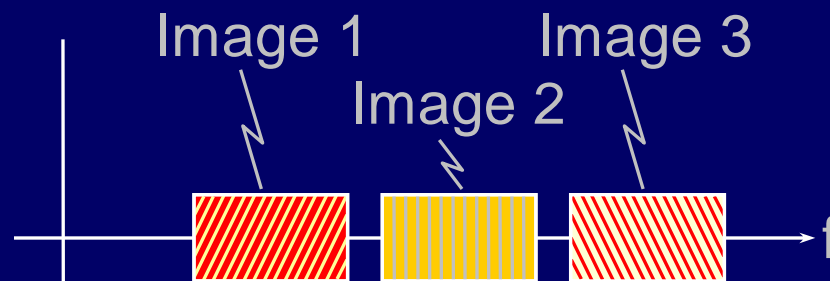
- 1) **Blur image** by averaging M^2 pixels $\Rightarrow Q = 0.53/M$
(using large B_τ signals yields high resolution, can be smoothed)
- 2) **Average using spatial diversity**



Reduction of SAR Speckle

Alternate ways to reduce “speckle” by average pixel intensities:

- 3) **Average using frequency diversity**, where each band yields an independent image. Note that the same total bandwidth could alternatively yield more range resolution and pixels for averaging.

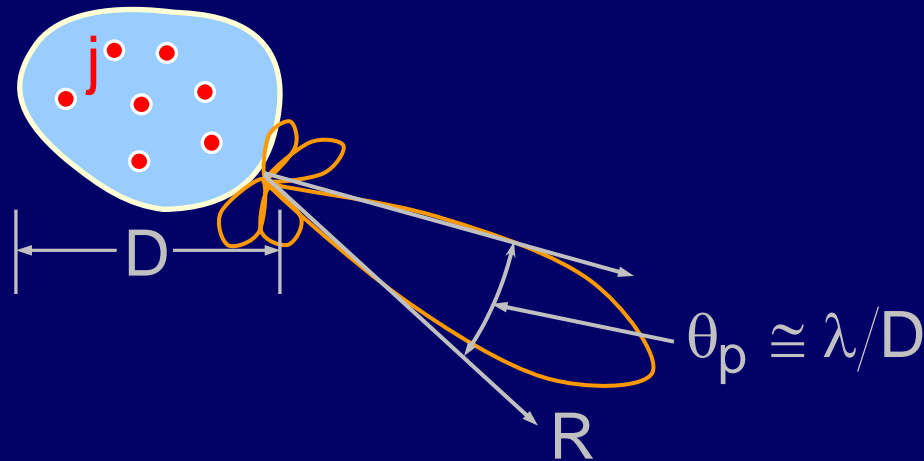


$$Q = \frac{0.53}{\sqrt{N}}$$

N Bands

Reduction of SAR Speckle

- 4) **Time averaging** works only if source varies. For example a narrow swath permits high PRF and an increase in N , but unless the antenna translates more than $\sim \lambda R/D$ between pulses [R = range, D = pixel width (m)], then adjacent pulse returns are correlated.

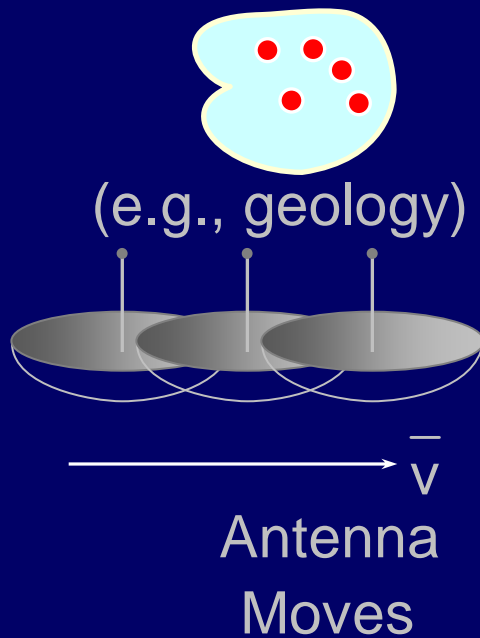


In general, reasonably smooth images need > 8 levels, so $Q' = S.D./M \cong (1/3)/4$ levels = $1/12$, versus $Q \cong 1/2$. To reduce standard deviation by 6, need $N \gtrsim 6^2 = 36$ looks.

Alternative SAR Geometries and Applications

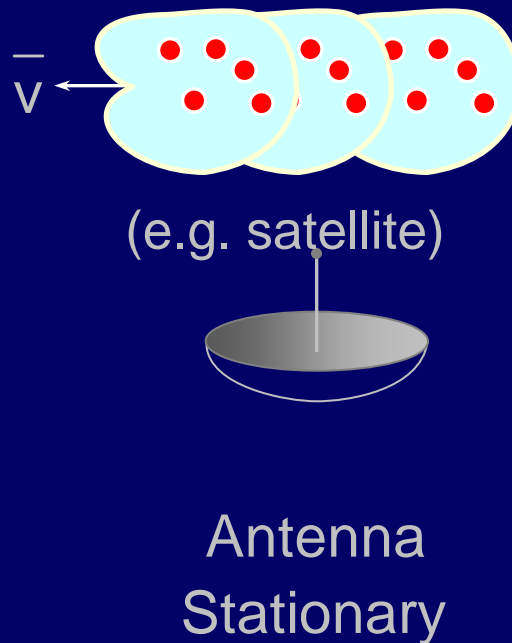
Case A.

Source Stationary



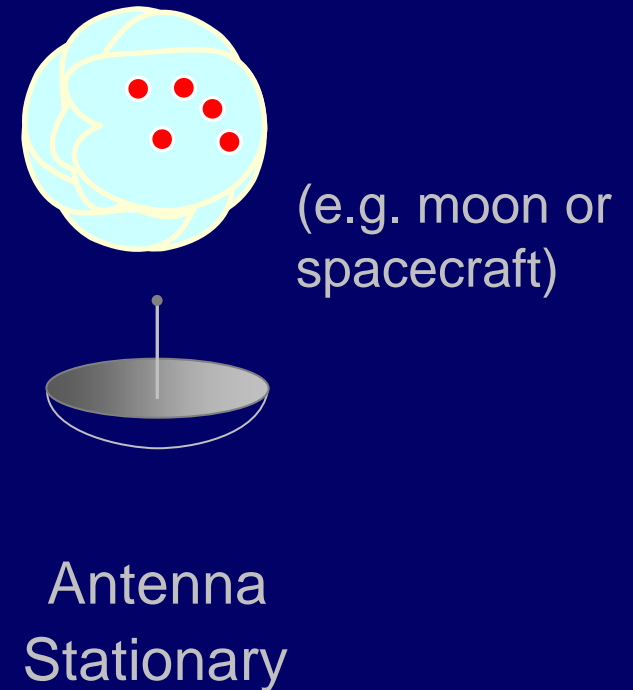
Case B.

Source Moves



Case C.

Source rotates



Velocity dispersion within inverse SAR (ISAR) source (e.g., a moving car) can displace its apparent position laterally.

ESTIMATION

Examples taken from Remote Sensing
Principles are Nonetheless Widely Applicable

Linear and Non-Linear Problems
Gaussian and Non-Gaussian Statistics

Professor David H. Staelin
Massachusetts Institute of Technology

Linear Estimation: Smoothing and Sharpening

Smoothing reduces image speckle and other noise; sharpening or “deconvolution” increases it.

Sharpening can “de-blur” images, compensating for diffraction or motion induced blurring.

Audio smoothing and sharpening are similar.

Consider antenna response example; we observe:

$$T_A(\bar{\psi}_A) = \frac{1}{4\pi} \int_{4\pi} G(\bar{\psi}_A - \bar{\psi}_s) T_B(\bar{\psi}_s) d\Omega_s$$

Linear Estimation: Smoothing and Sharpening

Consider antenna response example; we observe:

$$T_A(\bar{\psi}_A) = \frac{1}{4\pi} \int_{4\pi} G(\bar{\psi}_A - \bar{\psi}_s) T_B(\bar{\psi}_s) d\Omega_s$$

$$T_A(\bar{\psi}_A) \cong \frac{1}{4\pi} G(\bar{\psi}) * T_B(\bar{\psi}) \quad (\text{small solid angles})$$



$$\underline{T}_A(\underline{f}_\psi) = \frac{1}{4\pi} \underline{G}(\underline{f}_\psi) \bullet \underline{T}_B(\underline{f}_\psi)$$

\uparrow \uparrow
 Cycles/Radian Antenna Spectral Response

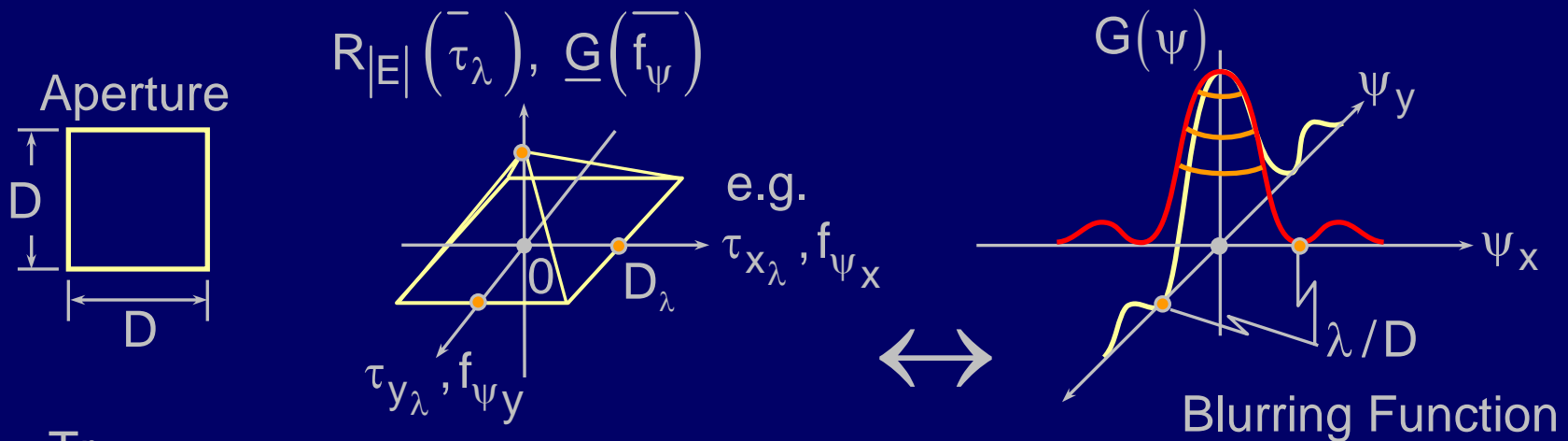
$$\left[\text{i.e., } \underline{G}(f_{\psi_x}, f_{\psi_y}) = \iint G(\psi_x, \psi_y) e^{-j2\pi(\psi_x f_{\psi_x} + \psi_y f_{\psi_y})} d\psi_x d\psi_y \right]$$

Example: Square Uniformly-Illuminated Aperture

$$T_A(\bar{\psi}_A) \cong \frac{1}{4\pi} G(\bar{\psi}) * T_B(\bar{\psi}) \quad (\text{small solid angles})$$

$$\underline{T}_A(\bar{f}_\psi) = \frac{1}{4\pi} \underline{G}(\bar{f}_\psi) \bullet \underline{T}_B(\bar{f}_\psi)$$

Cycles/Radian Antenna Spectral Response



Try:

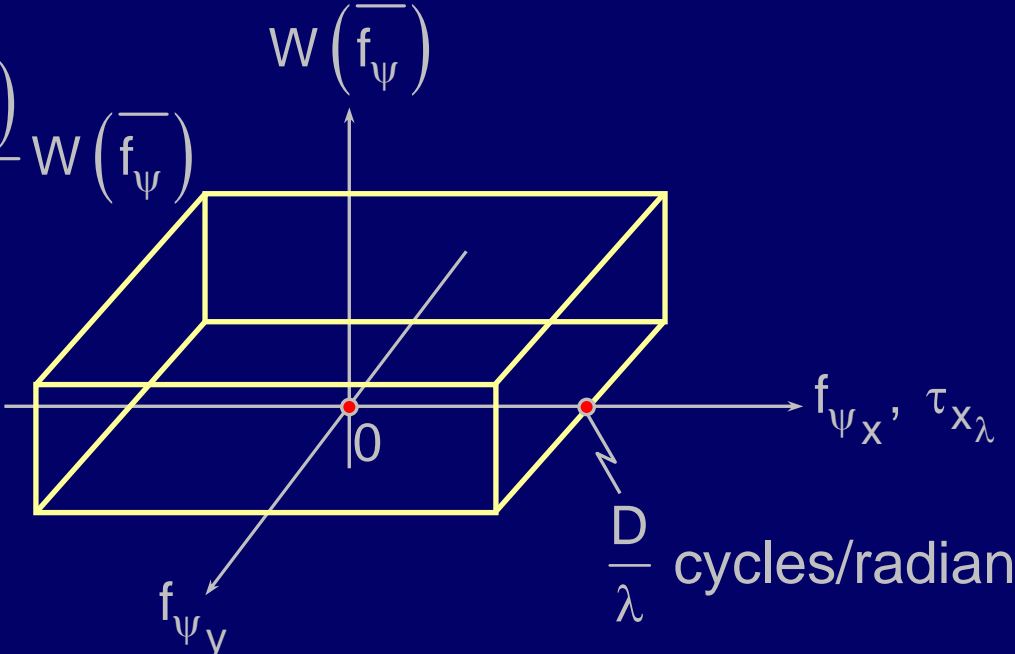
$$\hat{T}_B(\bar{f}_\psi) = \frac{4\pi \underline{T}_A(\bar{f}_\psi)}{\underline{G}(\bar{f}_\psi)}$$

This restores high-frequency components, but
 \leftarrow goes to zero for $|\bar{f}_{\psi x}| > D/\lambda!$

Example: Square Uniformly-Illuminated Aperture

$$\hat{T}_B(\bar{f}_\psi) = \frac{4\pi T_A(\bar{f}_\psi)}{\underline{G}(\bar{f}_\psi)} \quad \text{This restores high-frequency components, but}$$

$\underline{G}(\bar{f}_\psi) \leftarrow \text{goes to zero for } |\bar{f}_{\psi_x}| > D/\lambda!$

$$\text{Try: } \hat{T}_B(\bar{f}_\psi) = \frac{4\pi T_A(\bar{f}_\psi)}{\underline{G}(\bar{f}_\psi)} W(\bar{f}_\psi)$$


$\frac{D}{\lambda}$ cycles/radian

The window function $W(\bar{f}_\psi)$ avoids the singularity.

The "principal solution" uses a boxcar $W(s)$.

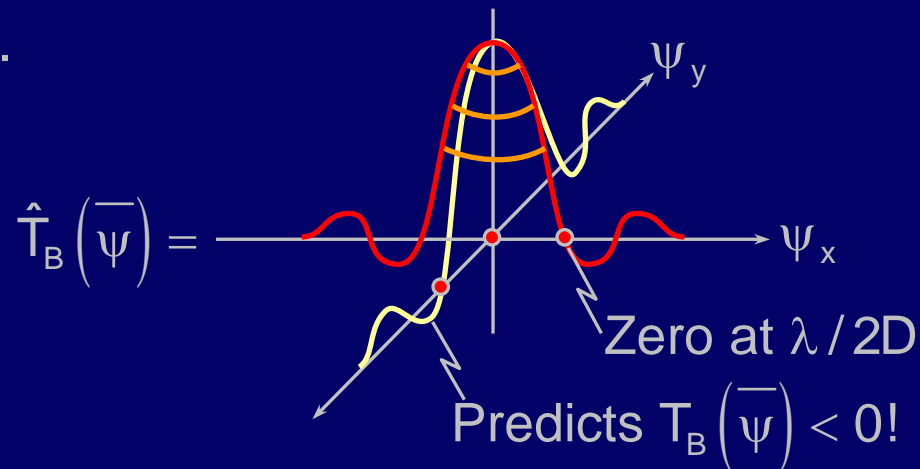
Example: Square Uniformly-Illuminated Aperture

Consider the restored (sharpened) image of a point source, $T_B(\bar{\psi}) = \delta(\bar{\psi})$:

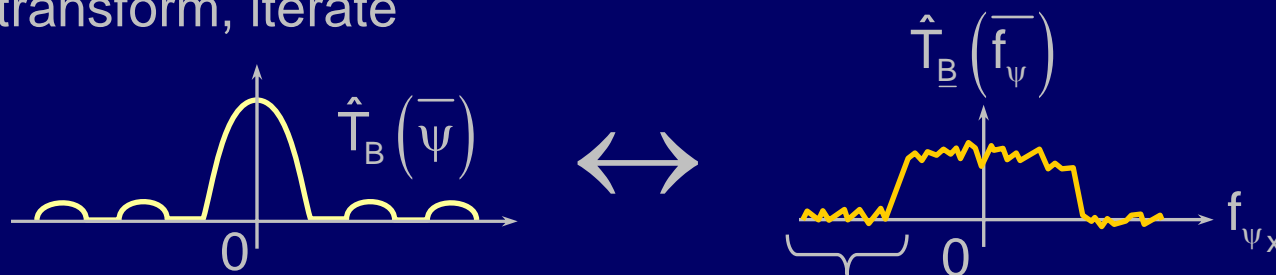
Then $T_{\underline{B}}(f_{\psi}) = 1$, so $\hat{T}_{\underline{B}}(\bar{f}_{\psi}) = 4\pi T_{\underline{A}}(\bar{f}_{\psi}) W(\bar{f}_{\psi}) / G(\bar{f}_{\psi}) = W(\bar{f}_{\psi})$,

since $T_A(\bar{f}_{\psi}) = G(\bar{f}_{\psi}) T_B(\bar{f}_{\psi}) / 4\pi$

$\hat{T}_B(\bar{\psi}) = 2\text{-D sinc function for a uniformly illuminated rectangular antenna aperture.}$



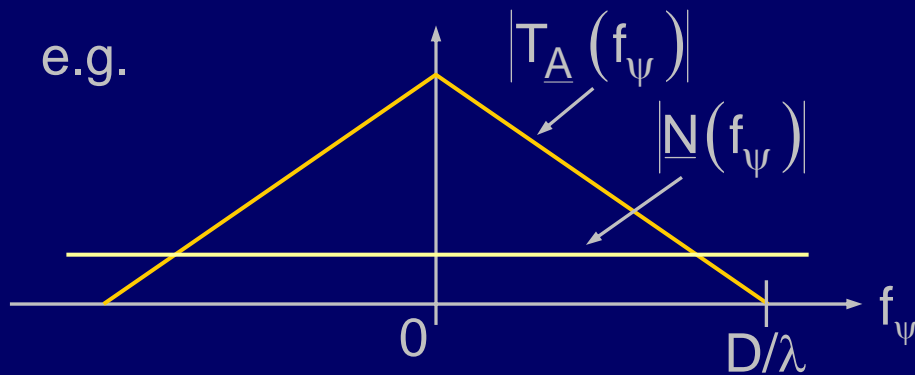
Can clip, transform, iterate



Sharpening Noisy Images

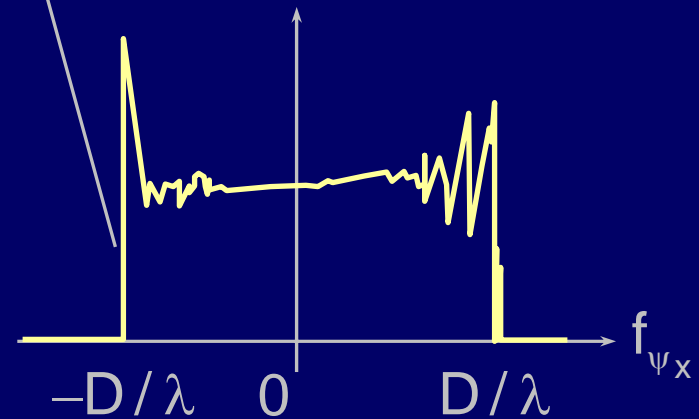
$$\hat{\underline{T}}_A(\underline{f}_\psi) = \underbrace{\underline{T}_A(\underline{f}_\psi)}_{\text{Truth}} + \underbrace{\underline{N}(\underline{f}_\psi)}_{\Delta T_{\text{rms}}}$$

e.g.



Amplifies white noise $\underline{N}(\underline{f}_\psi)$ for small $\underline{G}(\underline{f}_\psi)$

$\hat{\underline{T}}_B(\underline{f}_\psi)$
for point source



$\rightarrow 0!$ Amplifier Noise

$$\hat{\underline{T}}_B(\underline{f}_\psi) = \left[4\pi \hat{\underline{T}}_A(\underline{f}_\psi) / \underline{G}(\underline{f}_\psi) \right] W(\underline{f}_\psi)$$

Therefore optimize $W(\underline{f}_\psi)$

Sharpening Noisy Images

Therefore optimize $W(\bar{f}_\psi)$:

$$\text{Minimize } E \left[\left| \underline{T}_B(\bar{f}_\psi) - \frac{4\pi \underline{W}(\bar{f}_\psi)}{G(\bar{f}_\psi)} (\underline{T}_{A_0}(\bar{f}_\psi) + \underline{N}(\bar{f}_\psi)) \right|^2 \right] \stackrel{\Delta}{=} Q$$

$\partial Q / \partial W = 0$ yields:

$$\underline{W}(\bar{f}_\psi)_{\text{optimum}} = \frac{E \left[\left| \underline{T}_{A_0}(\bar{f}_\psi) \right|^2 + \frac{1}{2} \underline{T}_{A_0}(\bar{f}_\psi) \underline{N}(\bar{f}_\psi)^* + \frac{1}{2} \underline{T}_{A_0}^*(\bar{f}_\psi) \underline{N}(\bar{f}_\psi) \right]}{E \left[\left| \underline{T}_{A_0}(\bar{f}_\psi) + \underline{N}(\bar{f}_\psi) \right|^2 \right]}$$

If $E[\underline{T}_A \underline{N}] = 0$, then

$$\underline{W}_{\text{optimum}}(\bar{f}_\psi) = \frac{1}{1 + \frac{E \left[\left| \underline{N}(\bar{f}_\psi) \right|^2 \right]}{E \left[\left| \underline{T}_{A_0}(\bar{f}_\psi) \right|^2 \right]}} \left(\approx \frac{1}{1 + \frac{N}{S}} \right)$$

Sharpening Noisy Images

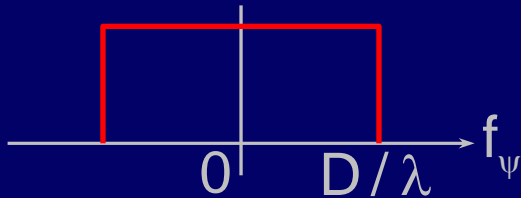
If $E[\underline{T}_A \underline{N}] = 0$, then

The weighting $(1 + N/S)^{-1}$ is widely used

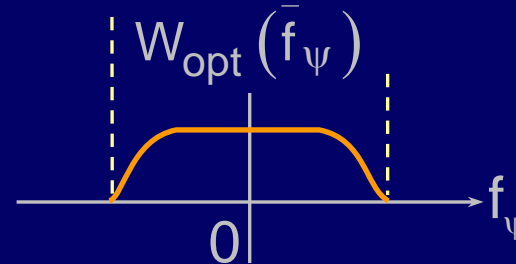
$$\underline{W}_{\text{optimum}}(\bar{f}_\psi) = \frac{1}{1 + \frac{E[|\underline{N}(\bar{f}_\psi)|^2]}{E[|\underline{T}_{A_0}(\bar{f}_\psi)|^2]}} \left(\cong \frac{1}{1 + \frac{N}{S}} \right)$$

$$\underline{W}_{\text{opt}}(\bar{f}_\psi)$$

for $\underline{N} = 0$:



$\underline{N} \neq 0$



$\underline{W}_{\text{opt}}(\bar{f}_\psi) \Rightarrow$ wider beam (lower spatial resolution), lower sidelobes.

Can be used for restoration of blurred images of all types:
 photographs TV, $\underline{T}_A(\bar{\psi}_A)$ maps, SAR images, filtered speech, etc.