

so we get

$$[A_i] = k_1 k_2 \dots k_{i-1} [A]_0 \cdot \sum_{j=1}^i d_j e^{-k_j t}$$

where d_j can not be determined in a general form.

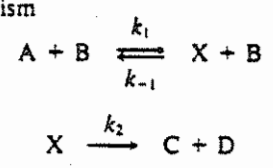
Note : if $k_1 = k_2 = \dots = k_n = k$

$$\sum [A_i] = \prod_{j=0}^{i-1} k_j [A]_0 \cdot \frac{1}{(p+k)^i}$$

$$[A_i] = k_1 \dots k_{i-1} [A]_0 \cdot \frac{[A_i]^{i-1} e^{-kt}}{(i-1)!}$$

2.4

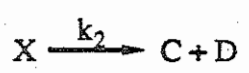
Consider the reaction mechanism



- (a) Write chemical rate equations for [A] and [X].
- (b) Employing the steady-state approximation, show that an effective rate equation for [A] is

$$\frac{d[A]}{dt} = -k_{eff} [A] [B]$$

- (c) Give an expression for k_{eff} in terms of k_1 , k_{-1} , k_2 , and [B].



(a) $\frac{d[A]}{dt} = -k_1 [A] [B] + k_{-1} [X] [B]$

$$\frac{d[X]}{dt} = +k_1 [A] [B] - k_{-1} [X] [B] - k_2 [X]$$

(b) let $\frac{d[X]}{dt} = 0$:

$$k_1 [A] [B] = k_{-1} [X] [B] + k_2 [X]$$

$$= (k_{-1} [B] + k_2) [X],$$

$$[X]_{ss} = \frac{k_1 [A] [B]}{k_{-1} [B] + k_2}$$

$$\frac{d[A]}{dt} = -k_1 [A] [B] + k_{-1} \left\{ \frac{k_1 [A] [B]}{k_{-1} [B] + k_2} \right\} [B]$$

$$= -k_1 [A] [B] + k_{-1} [A] [B] \left\{ \frac{k_1 [B]}{k_{-1} [B] + k_2} \right\}$$

$$= -k_{eff} [A] [B]; \text{ note } [B] \text{ is a constant}$$

(c) $-k_{eff} = +k_{-1} - k_1 \left\{ \frac{k_1 [B]}{k_{-1} [B] + k_2} \right\}$

$$= k_1 \left\{ 1 - \frac{k_1 [B]}{k_{-1} [B] + k_2} \right\}$$

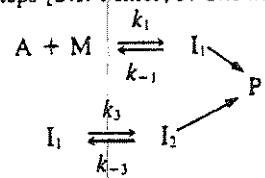
$$= k_1 \left\{ 1 - \frac{1}{1 + k_2/k_1 [B]} \right\}$$

$$= k_1 \left\{ \frac{1 + k_2/k_1 [B] - 1}{1 + k_2/k_1 [B]} \right\}$$

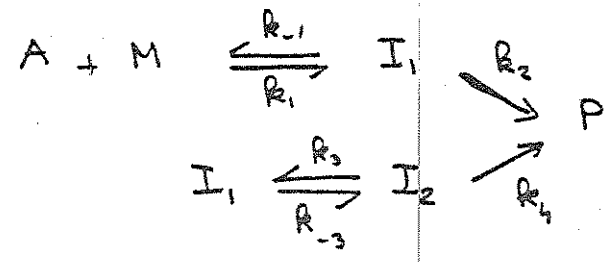
$$= \frac{k_1 k_2/k_1 [B]}{1 + k_2/k_1 [B]} = \frac{k_1 k_2}{k_{-1} [B] + k_2}$$

(equivalent expressions, in increasing order of elegance)

2.6 Consider a reaction with two intermediates I_1 and I_2 which both decompose to the same product P by competing parallel steps [S.I. Miller, *J. Chem. Education* 62, 490 (1985)]:



- (a) Find an expression for dP/dt by applying the steady state approximation with $[I_1]_{ss} = [I_2]_{ss} = 0$.
- (b) Find an expression for dP/dt by applying the steady state approximation with $[A]_t = [A]_0 - [I_1] - [I_2] - [P]$.
- (c) How do the expressions found in (a) and (b) differ, and what conclusions can be drawn from this difference?



a. Approximation with $[I_1] = [I_2] = 0$

$$\frac{d[I_1]}{dt} = k_1 [A][M] - k_{-1} [I_1] - k_2 [I_1] = 0$$

$$\frac{d[I_2]}{dt} = k_3 [I_1] - k_3 [I_2] - k_4 [I_2] = 0$$

$$\frac{d[P]}{dt} = k_2 [I_1] + k_4 [I_2]$$

$$[I_1] = k_1 \frac{[A][M]}{k_2 + k_{-1}}$$

$$[I_2] = \frac{k_3}{k_3 + k_4} [I_1]$$

from the two first steady-state approximation equations on I_1 and I_2

$$\frac{d[P]}{dt} = \frac{k_1 k_2}{k_2 + k_{-1}} [A][M] + \frac{k_4 k_3}{k_3 + k_4} [I_1]$$

$$\frac{d[P]}{dt} = \frac{k_1}{k_2 + k_1} [A][M] \left(k_3 + \frac{k_4 \cdot k_{-3}}{k_3 + k_4} \right)$$

b. Approximation with $[A] = [A]_0 - [I_1] - [I_2] - [P]$.

$$\frac{d[I_2]}{dt} \approx 0 \Leftrightarrow [I_2] = \frac{k_{-3}}{k_3 + k_4} [I_1]$$

$$\frac{d[I_1]}{dt} = k_1 [A][M] - k_{-1} [I_1] - k_2 [I_2]$$

$$= k_1 [A]_0 [M] - k_{-1} [M] [I_1] - k_2 [M] [I_2] - k_1 [M] [P] - k_{-1} [I_1] - k_2 [I_2]$$

$$= k_1 [M] ([A]_0 - [P]) - (k_{-1} [M] + k_1 + k_2) [I_1] - k_2 [M] [I_2]$$

$$= k_1 [M] ([A]_0 - [P]) - (k_{-1} [M] + k_1 + k_2) [I_1] - k_1 [M] \frac{k_{-3}}{k_3 + k_4} [I_1] \approx 0$$

$$[I_1] = \frac{k_1 [M] ([A]_0 - [P])}{k_{-1} [M] + k_1 + k_2 + \frac{k_1 k_{-3}}{k_3 + k_4} [M]}$$

$$\frac{d[P]}{dt} = k_2 [I_1] + k_4 [I_2]$$

$$\frac{d[P]}{dt} = \left(R_2 + \frac{R_4 R_3}{R_3 + R_4} \right) \frac{R_1 [M] ([A]_0 - [P])}{R_1 [M] + R_1 + R_2 + \frac{R_1 R_3}{R_3 + R_4} [M]}$$

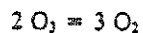
- c. If $[M]$ is almost constant, we can integrate the last equation which will provide $[P]$ as a function of time.

$$\frac{d[P]}{d - [P]} = R_2 dt. \quad \text{and so on.}$$

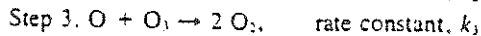
If $[M]$ is smaller enough that we can neglect all terms with $[M]$ in the denominator, then we'll get the first expression of $\frac{d[P]}{dt}$!

2.9

The mechanism for the decomposition of ozone into oxygen,



is stated to be as follows:



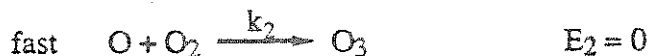
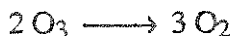
The activation energies, in kilojoules per mole, for each of the steps are as follows:

Step 1, $E_{\text{act}} = 103 \text{ kJ/mole}$

Step 2, $E_{\text{act}} = 0$

Step 3, $E_{\text{act}} = 21 \text{ kJ/mole}$

- (a) Obtain the differential equation for the steady state rate of decomposition of ozone, $-d[\text{O}_3]/dt$, in terms of the constants, k_1 , k_2 and k_3 , the concentration of ozone, $[\text{O}_3]$, and the concentration of oxygen, $[\text{O}_2]$.
- (b) On the basis of the values of E_{act} given above, simplify the expression for $-d[\text{O}_3]/dt$ obtained in (a) by eliminating any terms which can become negligible. State clearly the basis for the simplification.
- (c) Calculate the energy of activation for the overall reaction.



$$(a) \quad -\frac{d[\text{O}_3]}{dt} = k_1[\text{O}_3] - k_2[\text{O}][\text{O}_2] + k_3[\text{O}][\text{O}_3]$$

$$\frac{d[\text{O}]}{dt} = k_1[\text{O}_3] - k_2[\text{O}][\text{O}_2] - k_3[\text{O}][\text{O}_3] = 0 \text{ by steady-state approx.}$$

$$[\text{O}]_{\text{ss}} = \frac{k_1[\text{O}_3]}{k_2[\text{O}_2] + k_3[\text{O}_3]}$$

$$-\frac{d[\text{O}_3]}{dt} = k_1[\text{O}_3] - \frac{k_2 k_1 [\text{O}_2][\text{O}_3]}{k_2[\text{O}_2] + k_3[\text{O}_3]} + \frac{k_3 k_1 [\text{O}_3]^2}{k_2[\text{O}_2] + k_3[\text{O}_3]}$$

$$= \frac{k_1 k_2 [\text{O}_3][\text{O}_2] + k_1 k_3 [\text{O}_3]^2 - k_1 k_2 [\text{O}_2][\text{O}_3] + k_3 k_1 [\text{O}_3]^2}{k_2[\text{O}_2] + k_3[\text{O}_3]}$$

$$\boxed{-\frac{d[\text{O}_3]}{dt} = \frac{2 k_1 k_3 [\text{O}_3]^2}{k_2[\text{O}_2] + k_3[\text{O}_3]}}$$

- (b) It is assumed the O_2 , being the stable species, is as or more abundant than O_3 i.e. that

$$[O_2] \geq [O_3]$$

In addition, the energy of activation of the reverse reaction (2) is 0, while that of the forward reaction (3) is 21kJ/mole. Thus (2) has a temperature independent rate, while (3) has standard Arrhenius behavior. Thus at sufficiently low temperature $k_2 \gg k_3$ and we may rewrite the rate equation in the form

$$\frac{d[O_3]}{dt} = \frac{2k_1k_3[O_3]^2}{k_2[O_2]}$$

- (c) The overall rate constant is given by

$$k = \frac{2k_1k_3}{k_2} = \frac{2A_1A_3}{A_2} e^{-(E_1 + E_3 - E_2)/k_B T}$$

and the overall activation energy is

$$E_a^T = E_1 + E_3 - E_2 = \underline{124 \text{ kJ/mole}}$$

2.10

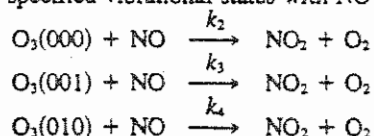
As a final variation on the theme of Problems 8 and 9, let us consider the reaction between NO and O_3 . In this experiment [E. Bar-Ziv, J. Moy, and R. J. Gordon, *J. Chem. Phys.* 68, 1013 (1978)], it is necessary to distinguish between ozone in its ground (000), excited stretching (001), and excited bending (010) vibrational states.

A CO_2 laser is used to excite ozone from the (000) to the (001) state. The following reactions then ensue in the presence of nitric oxide:

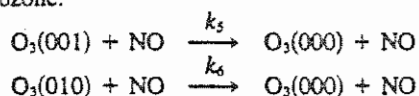
- (1) V-V equilibration of ozone:



- (2-4) reaction of ozone in specified vibrational states with NO to form NO_2 :



- (5,6) V-T relaxation of ozone:



The ozone (000) could be followed by its Hartley-band absorption at $\lambda = 254 \text{ nm}$, and the ozone (001) by its infrared emission at $\lambda = 9 \mu\text{m}$.

- (a) Write the kinetic equations, from the above (simplified) mechanism, for the time derivatives of $[O_3(000)]$, $[O_3(010)]$, $[O_3(001)]$, and $[NO_2]$. If the experiment is carried out in a large excess of NO, then pseudo-first-order kinetics may be obtained; rewrite these four expressions in pseudo-first-order, using $K_i = k_i[NO]$.
- (b) Find the Laplace transform of the four pseudo-first-order rate equations. (A table of Laplace transforms is included in the Appendix to Chapter 2.) Set up this set of transformed equations in determinantal form.
- (c) Find $[O_3(000)]_t$ and $[O_3(010)]_t$ in terms of pseudo-first-order rate coefficients derived from k_1 - k_6 and the initial concentrations of $O_3(000)$ and $O_3(001)$ following the laser pulse. Since the experiment is carried out at 300K, and $\nu_2 \approx 700 \text{ cm}^{-1}$ for ozone, the initial concentration of $[O_3(010)]$ cannot be neglected.

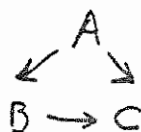
2-15 A somewhat different problem from the fully reversible cyclic mechanism in Problem 2.7 is the following system of reactions:

$$d[A]/dt = -k_1[A] - k_3[A]$$

$$d[B]/dt = k_1[A] - k_2[B]$$

$$d[C]/dt = k_2[B] + k_3[A]$$

which can be represented as



Using Laplace Transforms and/or a symbolic manipulation program such as MACSYMA or MATHEMATICA, find explicit expressions for $[A]_t$, $[B]_t$, and $[C]_t$ in terms of an initial concentration $[A]_0 = A_0$. Assume $[B]_0 = [C]_0 = 0$.

Equations 3-1, 3-2 and 3-3 are the differential equations that describe the concentrations of *N*-(phenylacetyl)glycyl-D-valine (A), glycyl-D-valine (B) and valine (C), respectively. After normalization, such that $A + B + C = 1$ at any time, the equation set

$$\frac{d[A]}{dt} = -k_1[A] - k_3[A] \quad (3-1)$$

$$\frac{d[B]}{dt} = k_1[A] - k_2[B] \quad (3-2)$$

$$\frac{d[C]}{dt} = k_2[B] + k_3[A] \quad (3-3)$$

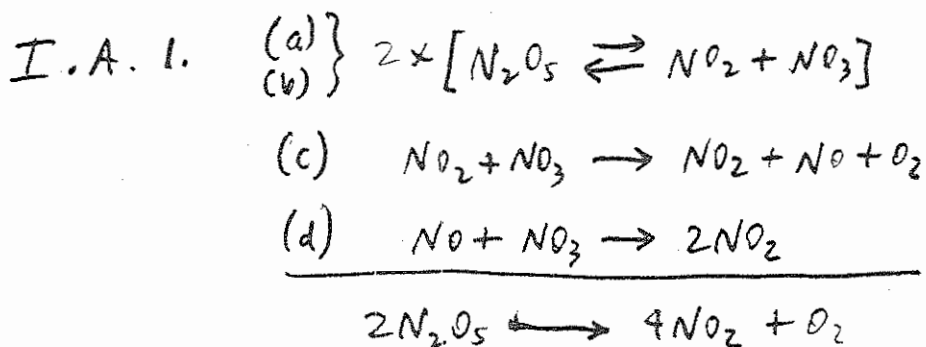
was solved using *Mathematica*¹⁰⁰ to give the following solutions. Equations 3-4, 3-5 and 3-6 describe the concentration, at a particular time, for *N*-(phenylacetyl)glycyl-D-valine, glycyl-D-valine and valine, respectively. Equation 3-4 was solved for a value of $(k_1 + k_3)$

$$[A]_t = \left(\frac{1}{e^{(k_1+k_3)t}} \right) (A_0) \quad (3-4)$$

$$[B]_t = \left(\frac{(-e^{k_2 t} + e^{(k_1+k_3)t})k_1}{e^{(k_1+k_2+k_3)t}(k_1 - k_2 + k_3)} \right) (A_0) \quad (3-5)$$

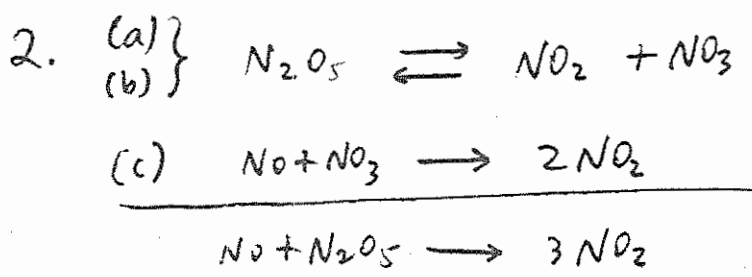
$$[C]_t = \left(\frac{-e^{(k_1+k_2)t}k_1 + e^{(k_1+k_2+k_3)t}k_1 + e^{k_2 t}k_2 - e^{(k_1+k_2+k_3)t}k_2 - e^{k_2 t}k_3 + e^{(k_1+k_2+k_3)t}k_3}{e^{(k_1+k_2+k_3)t}(k_1 - k_2 + k_3)} \right) (A_0) \quad (3-6)$$

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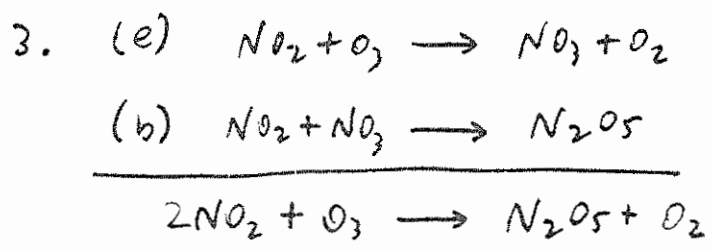


$c+d$ is equivalent to f , so $a+f$ OK

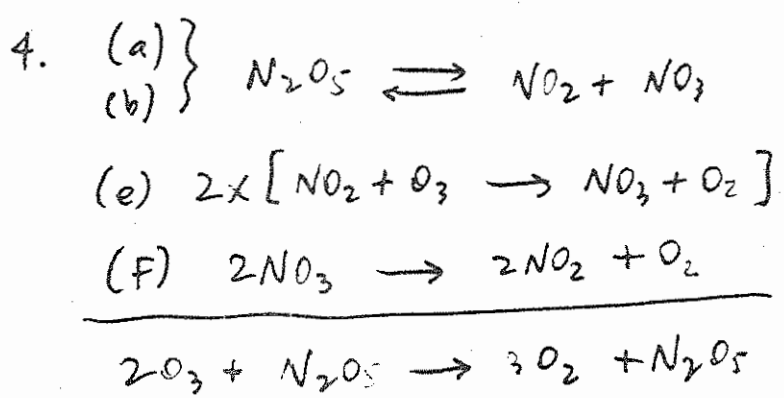
a, b, c, d

or
a, c, d


a, b, d



e, b



a, b, e, f

2. $R_4 = -\frac{1}{2} \frac{d[O_3]}{dt} = k_4 [N_2O_5]^{2/3} [O_3]^{2/3}$ by hypothesis.

$-\frac{d[O_3]}{dt} = k_e [O_3] [NO_2]$

$$\left. \begin{aligned} \frac{d[NO_2]}{dt} &= k_a [N_2O_5] - k_b [NO_2][NO_3] - k_c [NO_2][O_3] + 2k_f [NO_3]^2 = 0 \\ \frac{d[NO_3]}{dt} &= k_a [N_2O_5] - k_b [NO_2][NO_3] + k_c [NO_2][O_3] - 2k_f [NO_3]^2 = 0 \end{aligned} \right\} \text{steady state}$$

The $[N_2O_5]$ concentration is governed by (a) and (b),

$$[NO_2]_{ss} [NO_3]_{ss} = \left(\frac{k_a}{k_b}\right) [N_2O_5] = xy, \quad x = \left(\frac{k_a}{k_b}\right) [N_2O_5] / y = c/y$$

Thus

$$\begin{aligned} k_a [N_2O_5] - k_b xy - k_c x [O_3] + 2k_f y^2 &= 0 \\ - \{ k_a [N_2O_5] - k_b xy + k_c x [O_3] - 2k_f y^2 &= 0 \} \end{aligned}$$

$$-2k_c x [O_3] + 4k_f y^2 = 0$$

$$k_c (c/y) [O_3] = 2k_f y^2$$

$$k_c c [O_3] = 2k_f y^3$$

$$y = \left(\frac{k_c}{2k_f}\right)^{1/3} c^{1/3} [O_3]^{1/3} = \left(\frac{k_c}{2k_f}\right)^{1/3} \left(\frac{k_a}{k_b}\right)^{1/3} [N_2O_5]^{1/3} [O_3]^{1/3}$$

$$\begin{aligned} x = [NO_2]_{ss} &= \left(\frac{k_a}{k_b}\right) [N_2O_5] / \left(\frac{k_c}{2k_f}\right)^{1/3} \left(\frac{k_a}{k_b}\right)^{1/3} [N_2O_5]^{1/3} [O_3]^{1/3} \\ &= \left(\frac{2k_f}{k_c}\right)^{1/3} \left(\frac{k_a}{k_b}\right)^{2/3} [N_2O_5]^{2/3} [O_3]^{-1/3} \end{aligned}$$

$$\begin{aligned} - \frac{d[O_3]}{dt} &= k_c [O_3] [NO_2]_{ss} \\ &= k_c \left(\frac{2k_f}{k_c}\right)^{1/3} \left(\frac{k_a}{k_b}\right)^{2/3} [N_2O_5]^{2/3} [O_3]^{2/3} = 2k_4 [N_2O_5]^{2/3} [O_3]^{2/3} \end{aligned}$$

$$\therefore k_4 = 2^{-2/3} k_c^{2/3} k_f^{1/3} \left(\frac{k_a}{k_b}\right)^{1/3}$$