IV. Transport Phenomena Lecture 20: Warburg Impedance

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1. Warburg impedance for semi-infinite oscillating diffusion

Warburg (Ann. Physik. 1899) is credited with the first solution to the diffusion equation with oscillating concentration at the boundary, which is related to the diffusional (or mass transfer) impedance of electrochemical systems. An interesting point made in the first part of the class is that the very same mathematical model and impedance formula also holds for capacitive charging of a porous electrode with constant electrolyte concentration (i.e. no diffusion) modeled by an RC transmission line, and this effect is often mistaken for diffusional impedance.

We start by linearizing the equations for transport and electrochemical reactions to describe the response to a small oscillating voltage.

Suppose
$$\Delta V \sim \frac{k_B T}{ne} \ln \left(\frac{C_0 + \Delta C}{C_0} \right) \sim \frac{k_B T}{ne} \frac{\Delta C}{C_0}$$
 for linear response (e.g. Nernst equation, $\Delta C \ll C_0$) and $\Delta I \sim -neAD \frac{\partial C}{\partial x} (x=0)$

Also, assume quasi-equilibrium reactions at x=0 and linear diffusion.

$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial x^2}$$

Alternating current: $\Delta V = \operatorname{Re}[Ve^{iwt}]^{\operatorname{Re}alV} = V\cos(wt)$

$$\Delta I = \operatorname{Re}[Ie^{iwt}] = |I|\cos(wt + \varphi) \quad I = |I|e^{i\varphi}$$

$$\Delta C = C(x, t) - C_0 = \operatorname{Re}[Ce^{iwt}]$$

Therefore, iwC = DC''

Hence, $C = C(x=0)e^{-\sqrt{\frac{iw}{D}x}}$ ($C \to 0$ as $x \to \infty$)

$$\frac{C(x=0)}{-C'(x=0)} = \sqrt{\frac{D}{iw}}$$

Thus, impedance is

$$Z = \frac{\Delta V}{\Delta I} = \frac{k_B T}{(ne)^2 ADC_0} \frac{C(x=0)}{-C'(x=0)} = \frac{A}{\sqrt{iw}} A = \frac{k_B T}{(ne)^2 AC_0 \sqrt{D}}$$

This is the same result as an infinite RC transmission line because the mean potential satisfies the same form of linear diffusion equation.

2. Finite Length Warburg Impedance (FLW) for Fuel Cells

(also called "open boundary finite-length Warburg" impedance)

For oscillating diffusion layer, the characteristic length is $\Delta x \sim \sqrt{Dt} = \sqrt{\frac{D}{W}}$.



Now, $C=C_0$ is imposed on x=L, not at the infinity. At low frequency ($w \rightarrow 0$), FLW acts like a resistor. This situation is depicted in above figure.

Solve iwC = DC'' with C = 0 at x = L.

The general solution is
$$C = A \sinh\left[\sqrt{\frac{iw}{D}}(L-x)\right] + B \cosh\left[\sqrt{\frac{iw}{D}}(L-x)\right].$$

B = 0 due to C(x = L) = 0. Thus,

$$C = A \sinh\left[\sqrt{\frac{iw}{D}}(L-x)\right], \quad C' = -\sqrt{\frac{iw}{D}}A \cosh\left[\sqrt{\frac{iw}{D}}(L-x)\right]$$
$$\frac{C(x=0)}{-C'(x=0)} = \sqrt{\frac{D}{iw}} \tanh\left(\sqrt{\frac{iw}{D}}L\right)$$

Hence, the impedance is,

$$Z = \frac{\Delta V}{\Delta I} = \frac{k_B T}{(ne)^2 ADC_0} \frac{C(x=0)}{-C'(x=0)} = Z_0 \frac{1}{L} \sqrt{\frac{D}{iw}} \tanh\left(\sqrt{\frac{iw}{D}}L\right), \quad Z_0 = \frac{k_B T L}{(ne)^2 ADC_0}$$

$$\widetilde{Z} = \frac{Z}{Z_0}$$
 and $\widetilde{w} = \frac{wL^2}{D}$

Then, dimensionless impedance is

$$\widetilde{Z} = \frac{1}{\sqrt{i\widetilde{w}}} \tanh\left(\sqrt{i\widetilde{w}}\right) \sim \begin{cases} \frac{1}{\sqrt{i\widetilde{w}}} (\widetilde{w} >> 1) \\ 1 - \frac{i\widetilde{w}}{3} + \dots (\widetilde{w} << 1) \end{cases}$$

Hence, this is similar to the following circuit, except in the transition region:



The Nyquist plot is,



This behavior can be clearly seen in impedance spectra for PEM fuel cells, as shown in the next figure.



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Figure: (a) Nyquist plots of the impedance of a PEM fuel cell with a Nafion 113 membrane taken at different operating voltages (which leads to different surface concentrations, as explained in previous lectures). The data can be described well by the circuit in (b), where the low-frequency arc on the right comes from a finite-length Warburg impedance with resistance cutoff, given by the formula above. In this case, the double layer capacitance is replaced by a constant-phase element (CPE) attributed to RC transmission line effects, since it is distributed along a porous electrode/membrane interface.

3. FLW Impedance for Li-ion Batteries

(also called "blocked boundary finite-length Warburg impedance")

Now apply a zero flux Neuman BC at x=L instead of Dirichlet BC, to represent the finite end of intercalation particle. At higher frequency, this system has the same Warburg impedance as before. However, this system acts as a capacitor at low frequency at this time. Schematic figure is as follows.



Use the same notation as before. Then, dimensionless impedance is

$$\widetilde{Z} = \frac{1}{\sqrt{i\widetilde{w}}} \operatorname{coth}\left(\sqrt{i\widetilde{w}}\right) \sim \begin{cases} \frac{1}{\sqrt{i\widetilde{w}}} (\widetilde{w} >> 1) \\ \frac{i\widetilde{w}}{1} + \frac{1}{3} \dots (\widetilde{w} << 1) \end{cases}$$

This is similar to the following circuit except in the transition region





The last figure shows a clear example of the preceding model to describe the diffusion of lithium ions in silicon nanowires, used as anode intercalation material (due to their ability to accommodate the large elastic coherency strain associated with Li intercalation in silicon). The system is well described by a Randles circuit consisting of a parallel RC element for the double layers in series with a finite-length Warburg element for diffusion in the nanowires. By approximating each nanowire as 1D "pseudofilm" for diffusion, the formula above can be used to infer the diffusivity of lithium in silicon, e.g. from the limiting low-frequency resistance (=1/3 dimensionless).



Image by MIT OpenCourseWare.

Figure: Impedance spectrum (Nyquist plot) for a silicon nanowire anode in a Li-ion battery, which is well described by a parallel RC element for the double layer (high frequency "surface resistance") in series with a finite-length Warburg element with capacitive cutoff (low frequency "diffusion element").

10.626 Electrochemical Energy Systems Spring 2014

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