10.34: Numerical Methods Applied to Chemical Engineering

Lecture 19: Differential Algebraic Equations

- Differential algebraic equations
 - Semi-explicit
 - Fully implicit
- Simulation via backward difference formulas

- How suitable are such approaches?
- Consider stirred tank example I:

$$\begin{split} \frac{dc_2}{dt} &= \frac{Q}{V} \left(c_1(t) - c_2(t) \right) \\ c_1(t) &= \gamma(t) \\ \text{Apply backward Euler method:} \\ \frac{dx}{dt} \bigg|_{t_k} &= \frac{x(t_k) - x(t_{k-1})}{t_k - t_{k-1}} + O(t_k - t_{k-1}) \\ c_1(t_k) &= \gamma(t_k) \\ c_2(t_k) &= \frac{1}{1 + \frac{Q}{V}(t_k - t_{k-1})} \left(c_2(t_{k-1}) + \frac{Q}{V}(t_k - t_{k-1})c_1(t_k) \right) \\ &+ O((t_k - t_{k-1})^2) \end{split}$$

- How suitable are such approaches?
- Consider stirred tank example 2:

$$\frac{dc_2}{dt} = \frac{Q}{V} (c_1(t) \quad c_2(t))$$
$$c_2(t) = \gamma(t)$$

Apply backward Euler method:

$$c_2(t_k) = \gamma(t_k)$$

$$c_1(t_k) = c_2(t_k) + \frac{V}{Q} \left(\frac{c_2(t_k) - c_2(t_{k-1})}{t_k - t_{k-1}} \right) + O(t_k - t_{k-1})$$

- How suitable are such approaches?
- Consider the system of DAEs:

$$\dot{c}_2 = c_1(t)$$
$$\dot{c}_3 = c_2(t)$$
$$0 = c_3(t) - \gamma(t)$$

Apply backward Euler method:

$$c_{3}(t_{k}) = \gamma(t_{k})$$

$$c_{2}(t_{k}) = \frac{c_{3}(t_{k}) - c_{3}(t_{k-1})}{t_{k} - t_{k-1}} + O(t_{k} - t_{k-1})$$

$$c_{1}(t_{k}) = \frac{c_{2}(t_{k}) - c_{2}(t_{k-1})}{t_{k} - t_{k-1}} + O(1)!$$
5

- Solution via backward Euler:
 - Stirred-tank example I:
 - local truncation error: $O(\Delta t^2)$
 - Stirred-tank example 2:
 - local truncation error: $O(\Delta t)$
 - DAE example 3:
 - local truncation error: O(1)

- How suitable are such approaches?
- Consider the system of DAEs:

$$\dot{c}_1 = c_1(t) + c_2(t) + c_3(t)$$

$$\dot{c}_2 = -c_1(t) - c_2(t) + c_3(t)$$

$$0 = c_1(t) + c_2(t)$$

Apply backward Euler method:

• Consider stirred tank example I:

$$\frac{dc_2}{dt} = \frac{Q}{V} \left(c_1(t) - c_2(t) \right)$$
(I)
$$c_1(t) = \gamma(t)$$
(2)

 How many time derivatives are needed to convert to a system of independent ODEs having differentials of all the unknowns?

 $\frac{derivative of (2)}{dt} = \dot{\gamma}(t) \quad (3)$

Called an index-1 DAE.

• Consider stirred tank example 2:

$$\frac{dc_2}{dt} = \frac{Q}{V} \left(c_1(t) - c_2(t) \right)$$
(I)
$$c_2(t) = \gamma(t)$$
(2)

9

How many time derivatives are needed to convert to a $\frac{dc_2}{dt} = \dot{\gamma} \quad \rightarrow c_1(t) = c_2(t) + \frac{V}{Q}\dot{\gamma} \quad (3)$ rivative of (2) $\frac{dc_1}{dt} - \frac{dc_2}{dt} = \frac{V}{Q}\ddot{\gamma}$ index-2 DAE. $\frac{dc_1}{dt} - \frac{dc_1}{dt} = \frac{V}{Q}\ddot{\gamma} + \frac{Q}{V}(c_1(t) - c_2(t)) \quad (4)$ derivative of (2) Called an index-2 DAE.

Consider DAE example 3:

$$\dot{c}_2 = c_1(t)$$
 (I)
 $\dot{c}_3 = c_2(t)$ (2)
 $0 = c_3(t) - \gamma(t)$ (3)

How many time derivatives are needed to convert to a

system of ODEs? derivative of (3) substitute (2) $\dot{c}_3 = \dot{\gamma} \rightarrow c_2(t) = \dot{\gamma}$ (4) derivative of (4) $\dot{c}_2 = \ddot{\gamma} \rightarrow c_1(t) = \ddot{\gamma}$ (5) derivative of (5) $\dot{c}_1 = \ddot{\gamma}$ (6)

Called an index-3 DAE.

 The differential index of a semi-expicit DAE system is defined as the minimum number of differentiations required to convert the DAE to a system of independent ODEs.

$$0 = \frac{d\mathbf{g}}{dt} = \mathbf{g}^{(1)}(\mathbf{x}, \mathbf{y}, \dot{\mathbf{y}}, t)$$
$$\frac{d\mathbf{x}}{dt} = \mathbf{f}(\mathbf{x}, \mathbf{y}, t) \qquad 0 = \frac{d^2\mathbf{g}}{dt^2} = \mathbf{g}^{(2)}(\mathbf{x}, \mathbf{y}, \dot{\mathbf{y}}, t)$$
$$\vdots$$
$$\mathbf{solve for:}$$

$$\frac{d\mathbf{y}}{dt} = \mathbf{s}(\mathbf{x}, \mathbf{y}, t)$$

• Consider another example:

$$\dot{c}_1 = c_1(t) + c_2(t) + c_3(t)$$

$$\dot{c}_2 = -c_1(t) - c_2(t) + c_3(t)$$

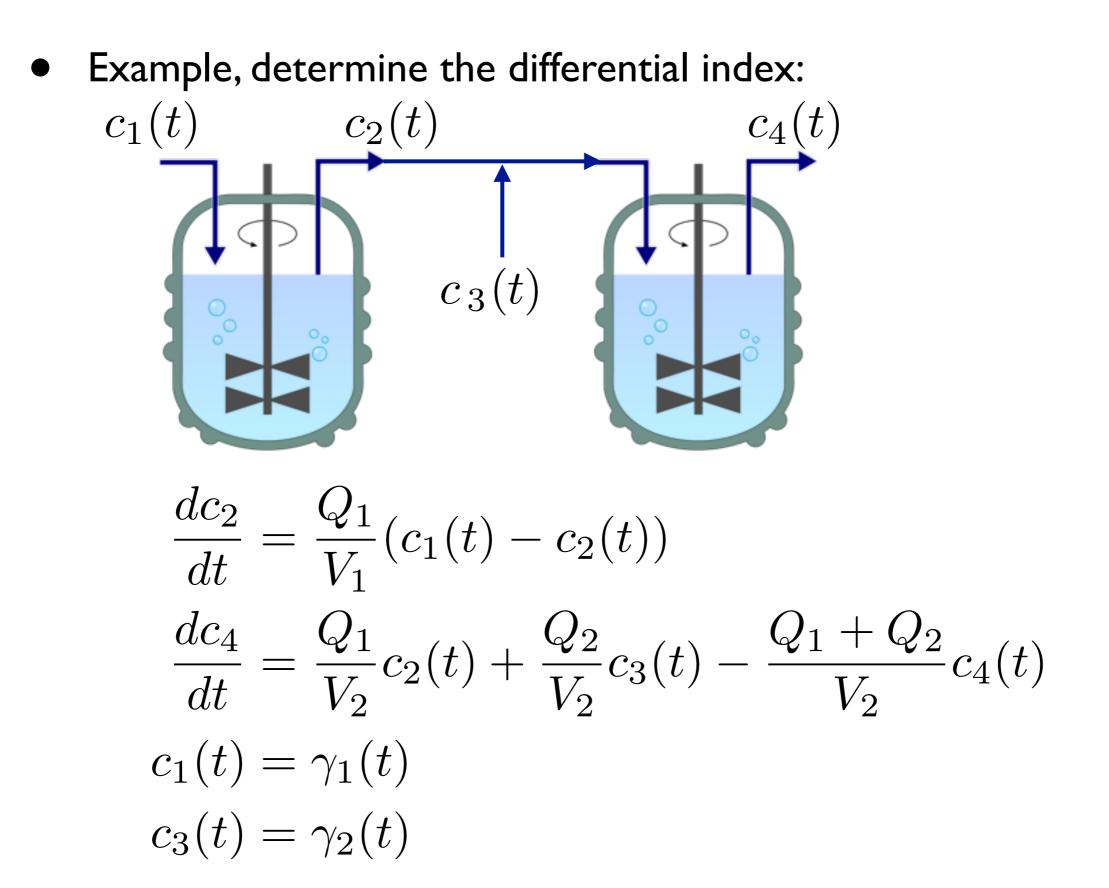
$$0 = c_1(t) + c_2(t)$$

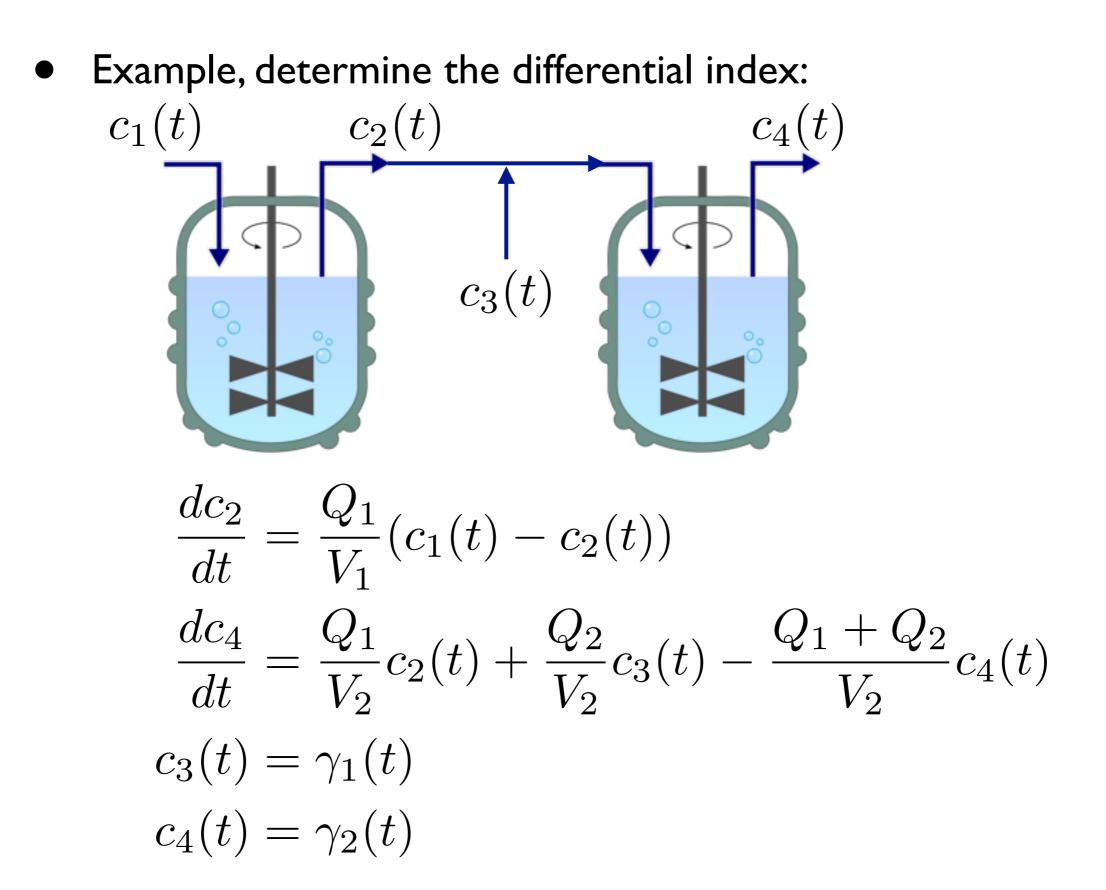
• How many time derivatives are needed to convert to a system of ODEs?

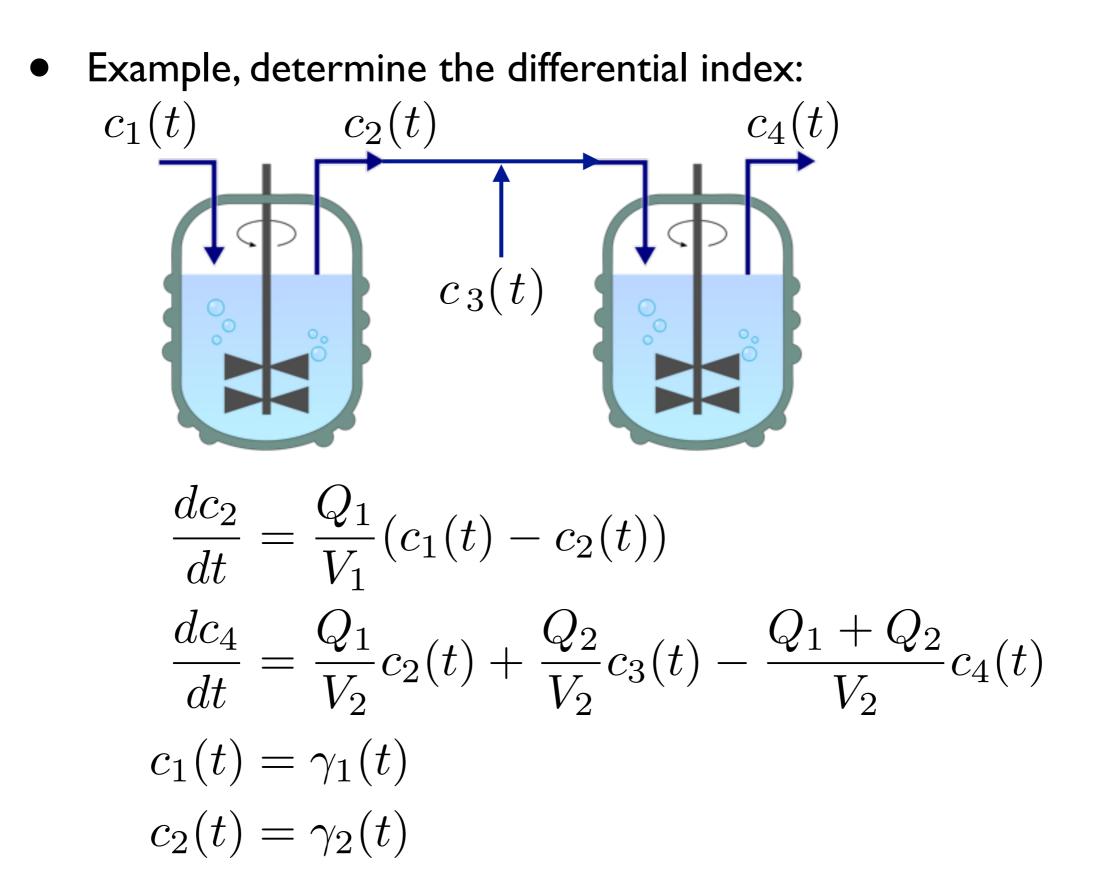
 The differential index of a semi-expicit DAE system is defined as the minimum number of differentiations required to convert the DAE to a system of ODEs.

$$\frac{d\mathbf{x}}{dt} = \mathbf{f}(\mathbf{x}, \mathbf{y}, t) (\mathbf{I})$$
$$0 = \mathbf{g}(\mathbf{x}, \mathbf{y}, t) (\mathbf{2})$$

 $\begin{aligned} \mathbf{derivative of (2)} & \text{rearrange and substitute (I)} \\ 0 &= \frac{d\mathbf{g}}{dt} = \frac{\partial \mathbf{g}}{\partial \mathbf{x}} \frac{d\mathbf{x}}{dt} + \frac{\partial \mathbf{g}}{\partial \mathbf{y}} \frac{d\mathbf{y}}{dt} + \frac{\partial \mathbf{g}}{\partial t} \xrightarrow{\mathbf{\partial}} \frac{\partial \mathbf{g}}{\partial \mathbf{y}} \frac{d\mathbf{y}}{dt} = -\frac{\partial \mathbf{g}}{\partial \mathbf{x}} \mathbf{f}(\mathbf{x}, \mathbf{y}, t) - \frac{\partial \mathbf{g}}{\partial t} \\ & \text{If } \frac{\partial \mathbf{g}}{\partial \mathbf{y}} \text{ is full rank then the DAE is index-I:} \\ & \frac{d\mathbf{y}}{dt} = -\left(\frac{\partial \mathbf{g}}{\partial \mathbf{y}}\right)^{-1} \left(\frac{\partial \mathbf{g}}{\partial \mathbf{x}} \mathbf{f}(\mathbf{x}, \mathbf{y}, t) + \frac{\partial \mathbf{g}}{\partial t}\right) \end{aligned}$







Dynamics of DAE Systems

- Solution of stirred tank example I: $c_2(t) = c_2(0)e^{-(Q/V)t}$ index I $c_1(t) = \gamma(t)$ $+ \frac{Q}{V} \int_0^t \gamma(t')e^{-(Q/V)(t-t')}dt'$
 - Solution of stirred tank example 2:

index 2
$$c_1(t) = \gamma(t) + \frac{V}{Q}\dot{\gamma}$$
 $c_2(t) = \gamma(t)$

• Solution of DAE example 3:

index 3
$$c_1(t) = \ddot{\gamma}$$
 $c_2(t) = \dot{\gamma}$ $c_3(t) = \gamma$

Higher index indicates greater sensitivity to changes in forcing function.

Dynamics of DAE Systems

• Physical example: pendulum

$$\begin{aligned} \dot{\mathbf{x}} &= \mathbf{v}(t) \\ m \dot{\mathbf{v}} &= -k(t)\mathbf{x}(t) + m\mathbf{g} \\ \|\mathbf{x}(t)\|_2^2 &= L^2 \end{aligned}$$

 \overline{m}

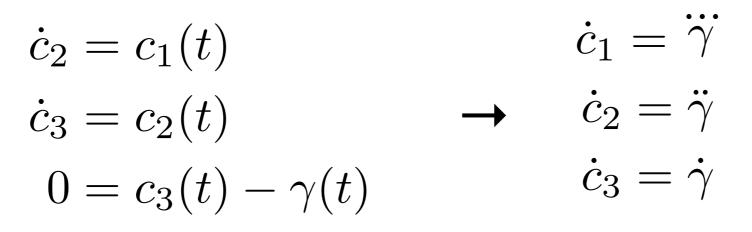
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- position, velocity, stiffness: $\mathbf{x}(t) \, \mathbf{v}(t) \, k(t)$
- Identify differential and algebraic variables. $\mathbf{x}(t) \mathbf{v}(t) \qquad k(t)$

• Identify index of the DAE system.
(1)
$$\frac{d}{dt} \|\mathbf{x}(t)\|_2^2 = 2\mathbf{v}(t) \cdot \mathbf{x}(t) = 0$$

(2) $\frac{d}{dt} (\mathbf{v}(t) \cdot \mathbf{x}(t)) = \frac{1}{m} (-k(t)\mathbf{x}(t) + m\mathbf{g}) \cdot \mathbf{x}(t) + \|\mathbf{v}(t)\|_2^2 = 0$
(3) $\frac{d}{dt} \left(\frac{1}{m} (-k(t)\mathbf{x}(t) + m\mathbf{g}) \cdot \mathbf{x}(t) + \|\mathbf{v}(t)\|_2^2 \right)$
 $= -\frac{1}{m} \frac{dk}{dt} \|\mathbf{x}(t)\|_2^2 - 2\frac{1}{m} k(t)\mathbf{v}(t) \cdot \mathbf{x}(t) + \mathbf{g} \cdot \mathbf{v} + \frac{2}{m} (-k(t)\mathbf{x}(t) + m\mathbf{g}) \cdot \mathbf{v}(t) = 0$ 18

• Consider DAE example 3:



• Can't I just solve the set of ODEs found when determining that the DAE system is index-3?

- In general, index-1 semi-explicit DAEs can be safely handled by certain stiff integrators in MATLAB (ode15s, ode23t)
- For generic DAEs, specific DAE solvers are usually needed (SUNDIALS, DAEPACK)
- Initial conditions for such equations must be prescribed consistently, or numerical errors can occur.
 - Consider the pendulum:
 - Can it's initial position be specified arbitrarily?
 - Can it's initial velocity be specified arbitrarily?
 - Can the initial stiffness be specified arbitrarily?

- Consistent initialization of initial value problems: $\{ \mathbf{\dot{x}}(0), \mathbf{x}(0) \}$
 - index-0 DAE (ODE-IVP): $\mathbf{\dot{x}} = \mathbf{f}(\mathbf{x}, t)$
 - I. $\mathbf{x}(0) \rightarrow \mathbf{\dot{x}}(0) = \mathbf{f}(\mathbf{x}(0), 0)$
 - 2. $\dot{\mathbf{x}}(0)$ solve $\dot{\mathbf{x}}(0) = \mathbf{f}(\mathbf{x}(0), 0)$
 - 3. $\mathbf{c}(\mathbf{x}(0), \mathbf{\dot{x}}(0)) = 0$ solve with $\mathbf{\dot{x}}(0) = \mathbf{f}(\mathbf{x}(0), 0)$
 - fully implicit DAE: $\mathbf{f}(\mathbf{x}, \mathbf{\dot{x}}, t) = 0$
 - 2N unknowns for N equations
 - apparently N degrees of freedom to specify
 - hidden constraints reduce these degrees
 - with differential states x and algebraic states y, $\mathbf{f}(\mathbf{\dot{x}}, \mathbf{x}, \mathbf{y}, t) = 0$ { $\mathbf{\dot{x}}(0), \mathbf{x}(0), \mathbf{y}(0)$ }

Consistent initialization, example stirred tank I:

$$\frac{dc_2}{dt} = \frac{Q}{V} (c_1(t) - c_2(t))$$
(I)
$$c_1(t) = -(t)$$
(2)

Convert to system of ODFs

$$\frac{dc_1}{dt} = \cdot (t)$$

$$\frac{dc_2}{dt} = \frac{Q}{V} (c_1(t) - c_2(t)) \quad (3)$$

$$\begin{array}{l} \text{Constrained by} \\ \text{algebraic equation (2)} \\ c_1(0) = \gamma(0) \end{array} \quad \begin{array}{l} \text{constrained by} \\ \dot{c}_2(0) = \frac{Q}{V} (c_1(0) - c_2(0)) \\ \dot{c}_2(0) = c_0 \end{array}$$

 $c_1(0)$

• Consistent initialization, example stirred tank 2:

$$\frac{dc_2}{dt} = \frac{Q}{V} \left(c_1(t) - c_2(t) \right) \quad (\mathbf{I})$$
$$c_2(t) = \gamma(t) \qquad (\mathbf{2})$$

Convert to system of ODEs

$$\frac{dc_2}{dt} = \dot{\gamma} \tag{3}$$

$$\frac{dc_1}{dt} = \frac{V}{Q}\ddot{\gamma} + \frac{Q}{V}(c_1(t) - c_2(t))$$

Consistent initial conditions:

constrained by differential equation (1) $c_1(0) = c_2(0) + \frac{V}{Q}\dot{c}_2(0)$ constrained by $\dot{c}_2(0) = \dot{\gamma}(0)$ $\dot{c}_2(0) = \dot{\gamma}(0)$

constrained by algebraic equation (2) $c_2(0) = \gamma(0)$

• Consider another example:

$$\dot{c}_1 = c_1(t) + c_2(t) + c_3(t)$$
$$\dot{c}_2 = -c_1(t) - c_2(t) + c_3(t)$$
$$0 = c_1(t) + c_2(t)$$

• Derive consistent initial conditions:

• Consider another example:

$$\dot{c}_1 = c_1(t) + c_2(t) + c_3(t)$$

$$\dot{c}_2 = -c_1(t) - c_2(t) + c_3(t)$$

$$0 = c_1(t) + c_2(t) + 2c_3(t)$$

• Derive consistent initial conditions:

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