

Last time: Strain energy density function
 Linear viscoelasticity
 - creep
 - stress relaxation
 - oscillatory testing

Lumped parameter models:

- Maxwell



$$F_1 = k u_1$$

spring → elastic



$$F_2 = \eta \frac{du_2}{dt}$$

dashpot → viscous



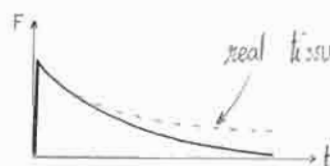
□ Lumped parameter models

Maxwell

$$\left. \begin{aligned} u &= u_1 + u_2 \\ F &= F_1 = F_2 \end{aligned} \right\}$$

$$k \frac{du}{dt} = \frac{dF}{dt} + \frac{k}{\eta} F$$

• stress relaxation



real tissue not very well described by Maxwell model

• limitations of the Maxwell model:

- stress relaxes to zero
- creep not like most material

• creep

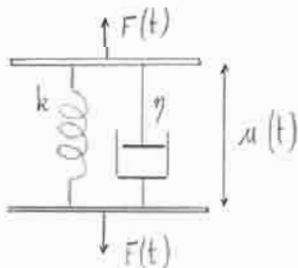


note: F related to stress σ & displacement u related to strain ϵ

Try another model with paradigm:

- choose model that fits experimental behavior
- determine $k_1, \dots, \eta_1, \dots$
- relate to microscopic behavior

Voigt

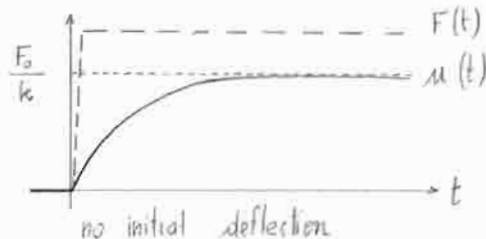


$$\left. \begin{aligned} u &= u_1 = u_2 \\ F &= F_1 + F_2 \\ &= k u + \eta \frac{du}{dt} \end{aligned} \right\}$$

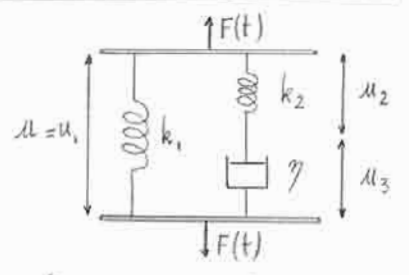
$$\frac{F}{\eta} = \frac{k}{\eta} u + \frac{du}{dt}$$

• creep: given forcing step function for F, find u(t)
 Solution to the constitutive equation:

$$\left. \begin{aligned} u(t) &= \frac{F_0}{k} \left(1 - \exp\left(-\frac{t}{\tau_R}\right) \right) \\ \tau_R &= \eta/k \end{aligned} \right\}$$



Kelvin or "standard linear solid"



$$\left. \begin{aligned} u &= u_1 = u_2 + u_3 \\ \dot{F} &= F_1 + F_2 \\ F_2 &= F_3 \end{aligned} \right\}$$

$$F + \alpha \frac{dF}{dt} = k_1 u + \beta \frac{du}{dt}$$

In pb set #5, find α & β in terms of k_1, k_2 & η

The standard linear solid exhibits creep & stress relaxation similar to most biological tissues

Continue to add elements $k_1, k_2, \dots, k_n, \eta_1, \eta_2, \dots, \eta_m$

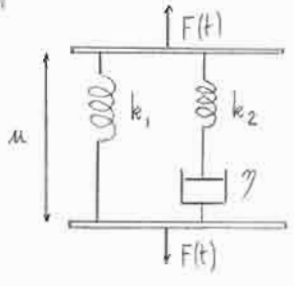
each one corresponds to a characteristic relaxation time

you can fit about anything, but what do you learn about your biological tissue?

Dynamic oscillatory behavior

(transient behavior, sinusoidal steady-state)

example of the 3-element model



input $u(t) = u_0 \cos \omega t = \text{Re} [u_0 e^{i\omega t}]$

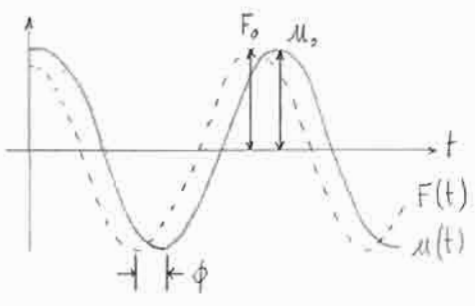
$$e^{i\omega t} = \cos(\omega t) + i \sin(\omega t)$$

output $F(t) = \text{Re} [\hat{F}(\omega) e^{i\omega t}] = \text{Re} [|\hat{F}| e^{i\phi} e^{i\omega t}]$

function of ω, k_1, k_2, η $F_0 \exp(i(\omega t + \phi))$

$$F(t) = F_0 \cos(\omega t + \phi)$$

define a complex modulus



$$\hat{G}(\omega, k_1, k_2, \eta) = \frac{\hat{F}(\omega)}{u_0} = \frac{|\hat{F}| e^{i\phi}}{u_0} = \frac{F_0(\omega)}{u_0} (\cos \phi + i \sin \phi)$$

$$G' \text{ storage modulus} = \frac{F_0(\omega)}{u_0} \cos \phi$$

$$G'' \text{ loss modulus} = \frac{F_0(\omega)}{u_0} \sin \phi$$

$$\hat{G} = G' + i G'' \quad \text{and} \quad \frac{G''}{G'} = \tan \phi$$

Experiment: measure frequency-dependence of G' and G'' (or phase lag ϕ) and infer values for k_1, k_2, η , and finally relate them to molecular behavior.

For SLS model

$$F + \alpha \frac{dF}{dt} = k_1 u + \beta \frac{du}{dt} \quad \text{and} \quad \frac{d}{dt} \leftrightarrow i\omega$$

$$\hat{F}(\omega) (1 + i\alpha\omega) e^{i\omega t} = u_0 (k_1 + i\beta\omega) e^{i\omega t}$$

we have $\hat{G}(\omega) = \frac{\hat{F}(\omega)}{u_0} = G' + i G''$

$$= \frac{k_1 + i\beta\omega}{1 + i\alpha\omega} = \frac{(k_1 + i\beta\omega)(1 - i\alpha\omega)}{(1 + i\alpha\omega)(1 - i\alpha\omega)} = \underbrace{\frac{k_1 + \alpha\beta\omega^2}{1 + \alpha^2\omega^2}}_{G'} + i \underbrace{\frac{(\beta - k_1\alpha)\omega}{1 + \alpha^2\omega^2}}_{G''}$$



low ω or long time
high ω or short time

at low frequency { dashpot has no effect because has plenty of time to respond
only k_1 counts, thus $G' = k_1$ (all force released in k_2 by η)
loss modulus governed by dashpot in the middle
very low dissipation when dashpot neglected.

at high frequency { dashpot doesn't have time to respond, only the two springs count
no role for dashpot hence $G'' \rightarrow 0$
 k_1 and k_2 act together, so $G' = k_1 + k_2$

the critical frequency where dashpot plays a role with $\omega_c \sim \frac{k_1}{\eta}$