# Unit 21 Influence Coefficients

## Readings:

Rivello 6.6, 6.13 (again), 10.5

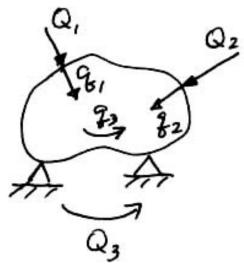
Paul A. Lagace, Ph.D. Professor of Aeronautics & Astronautics and Engineering Systems Have considered the vibrational behavior of a discrete system. How does one use this for a continuous structure?

First need the concept of.....

### **Influence** Coefficients

which tell how a force/displacement at a particular point "influences" a displacement/force at another point

- --> useful in matrix methods...
  - finite element method
  - lumped mass model (will use this in next unit)
- --> consider an arbitrary elastic body and define:
- Figure 21.1 Representation of general forces on an arbitrary elastic body



q<sub>i</sub> = generalized displacement (linear or rotation)

 $Q_i$  = generalized force (force or moment/torque)

Note that  $Q_i$  and  $q_i$  are:

- at the same point
- have the same sense (i.e. direction)
- of the same "type"

(force ↔ displacement) (moment ↔ rotation)

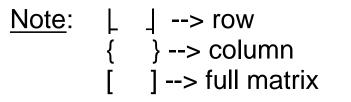
For a linear, elastic body, superposition applies, so can write:

$$q_{i} = C_{ij} Q_{j} \begin{cases} q_{1} = C_{11} Q_{1} + C_{12} Q_{2} + C_{13} Q_{3} \\ q_{2} = C_{21} Q_{1} + C_{22} Q_{2} + C_{23} Q_{3} \\ q_{3} = C_{31} Q_{1} + C_{32} Q_{2} + C_{33} Q_{3} \end{cases}$$

or in Matrix Notation:

$$\begin{cases} q_1 \\ q_2 \\ q_3 \end{cases} = \begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & C_{32} & C_{33} \end{bmatrix} \begin{cases} Q_1 \\ Q_2 \\ Q_3 \end{cases}$$

Paul A. Lagace © 2001



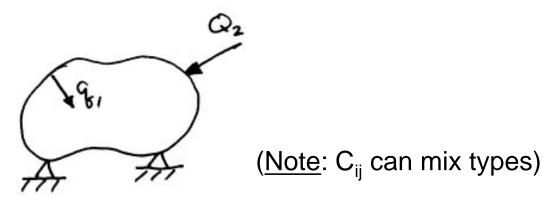
or

C<sub>ii</sub> = <u>Flexibility Influence Coefficient</u>

and it gives the deflection at i due to a unit load at j

 $C_{12}$  = is deflection at 1 due to force at 2

Figure 21.2 Representation of deflection point 1 due to load at point 2

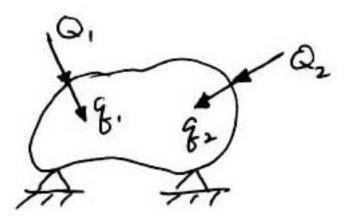


### Very important theorem:

# Maxwell's Theorem of Reciprocal Deflection

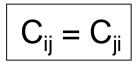
(Maxwell's Reciprocity Theorem)

*Figure 21.3* Representation of loads and deflections at two points on an elastic body



q<sub>1</sub> due to unit load at 2 is <u>equal</u> to q<sub>2</sub> due to unit load at 1 i.e.  $C_{12} = C_{21}$ 

Generally:



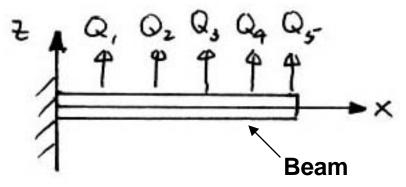
symmetric

This can be proven by energy considering (path independency of work)

--> Application of Flexibility Influence Coefficients

Look at a beam and consider 5 points...

Figure 21.4 Representation of beam with loads at five points



The deflections  $q_1...q_5$  can be characterized by:

$$\begin{cases} q_1 \\ q_2 \\ q_3 \\ q_4 \\ q_5 \end{cases} = \begin{bmatrix} C_{11} & C_{12} & C_{13} & C_{14} & C_{15} \\ C_{21} & C_{22} & \cdots & \cdots & \vdots \\ \vdots & & \ddots & & \vdots \\ \vdots & & & \ddots & & \vdots \\ C_{51} & \cdots & \cdots & C_{55} \end{bmatrix} \begin{bmatrix} Q_1 \\ Q_2 \\ Q_3 \\ Q_4 \\ Q_5 \end{bmatrix}$$

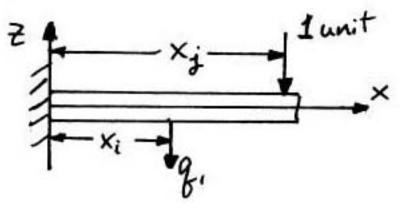
Since  $C_{ij} = C_{ji}$ , the  $[C_{ij}]$  matrix is <u>symmetric</u>

Thus, although there are 25 elements to the C matrix in this case, only 15 need to be computed.

So, for the different loads  $Q_1 \dots Q_5$ , one can easily compute the  $q_1 \dots q_5$  from previous work...

Example: C<sub>ii</sub> for a Cantilevered Beam

Figure 21.5 Representation of cantilevered beam under load



find: C<sub>ii</sub> --> deflection at i due to unit load at j

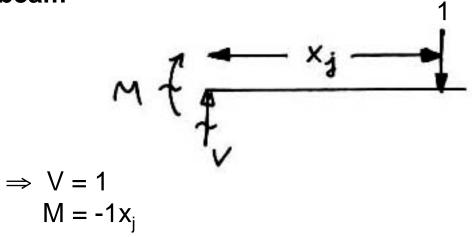
- Most efficient way to do this is via Principle of Virtual Work (energy technique)
- Resort here to using simple beam theory:

$$EI\frac{d^2w}{dx^2} = M(x)$$

### What is M(x)?

--> First find reactions:

*Figure 21.6* Free body diagram to determine reactions in cantilevered beam



--> Now find M(x). Cut beam short of  $x_i$ :

Figure 21.7 Free body diagram to determine moment along cantilevered beam

$$\sum M_x = 0 +$$
  

$$\Rightarrow 1 \cdot x_j - 1 \cdot x + M(x) = 0$$
  

$$\Rightarrow M(x) = -1(x_j - x)$$

Plugging into deflection equation:

$$EI\frac{d^2w}{dx^2} = -1\left(x_j - x\right)$$

for EI constant:

$$\frac{dw}{dx} = -\frac{1}{EI} \left( x_j x - \frac{x^2}{2} \right) + C_1$$
$$w = -\frac{1}{EI} \left( x_j \frac{x^2}{2} - \frac{x^3}{6} \right) + C_1 x + C_2$$

**Boundary Conditions:** 

Paul A. Lagace © 2001

So:

$$w = -\frac{1}{EI} \left( x_j \frac{x^2}{2} - \frac{x^3}{6} \right)$$

evaluate at x<sub>i</sub>:

$$w = \frac{1}{2EI} \left( \frac{x_i^3}{3} - x_i^2 x_j \right)$$

One important note:

w is defined as positive up, have defined  $q_i$  as positive down. So:

$$q_i = -w = \frac{1}{2EI} \left( x_i^2 x_j - \frac{x_i^3}{3} \right)$$

$$\Rightarrow \boxed{C_{ij} = \frac{1}{EI} \left( \frac{x_i^2 x_j}{2} - \frac{x_i^3}{6} \right)}_{for x_i \le x_j}$$
 for  $x_i \le x_j$ 

Deflection,  $q_i$ , at  $x_i$  due to unit force,  $Q_j$ , at  $x_j$ 

--> What about for  $x_i \le x_j$ ? Does one need to go through this whole procedure again?

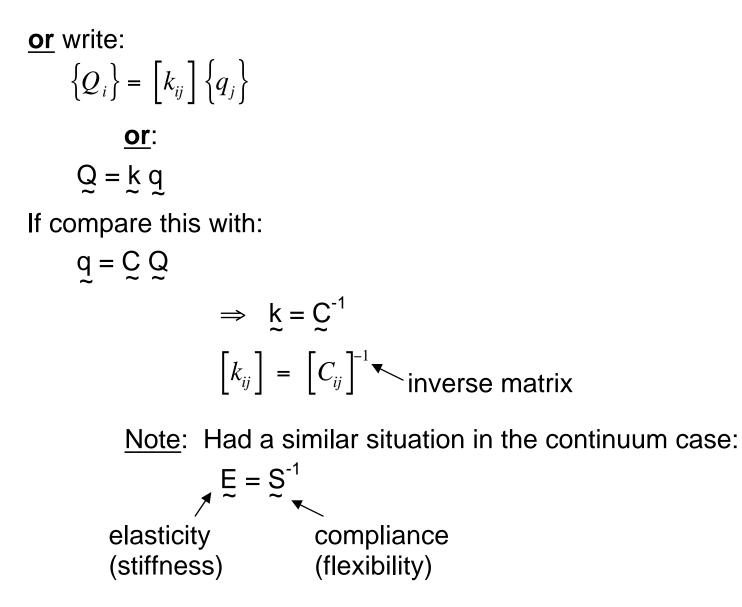
<u>No</u>! Can use the <u>same</u> formulation due to the symmetry of  $C_{ij}$ ( $C_{ii} = C_{ii}$ )

--> Thus far have looked at the influence of a force on a displacement. May want to look at the "opposite": the influence of a displacement on a force. Do this via...

# Stiffness Influence Coefficients = k<sub>ij</sub>

where can write:

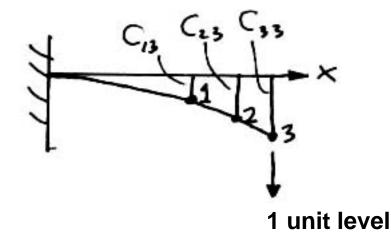
$$Q_{1} = k_{11}q_{1} + k_{12}q_{2} + k_{13}q_{3}$$
$$Q_{2} = k_{21}q_{1} + k_{22}q_{2} + k_{23}q_{3}$$
$$Q_{3} = k_{31}q_{1} + k_{32}q_{2} + k_{33}q_{3}$$



--> Look at the Physical Interpretations:

#### Flexibility Influence Coefficients

Figure 21.8 Physical representation of flexibility influence coefficients for cantilevered beam

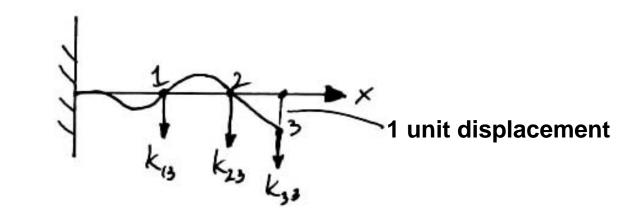


 $C_{ii}$  = displacement at i due to unit load at j

<u>Note</u>: This is only defined for <u>sufficiently</u> <u>constrained</u> structure

#### Stiffness Influence Coefficients

Figure 21.9 Physical representation of stiffness influence coefficients for cantilevered beam



 $k_{ij}$  = forces at i's to give a unit displacement at j and <u>zero</u> displacement everywhere else (at nodes)

(much harder to think of than C<sub>ii</sub>)

<u>Note</u>: This can be defined for unconstrained structures

- --> Can find k<sub>ii</sub> by:
  - calculating  $[C_{ij}]$  first, then inverting

$$k_{ij} = \frac{(-1)^{i+j}}{|\Delta|} \begin{vmatrix} \min \sigma & \sigma \\ C_{ij} \end{vmatrix}$$
  
determinant of  $[C_{ij}]$ 

- <u>Note</u>: k<sup>-1</sup> may be singular (indicates "rigid body" modes) --> rotation --> translation --> etc.
- calculating [k<sub>ij</sub>] directly from individual local [k<sub>ij</sub>] elements and adding up for the total system

Most convenient way

<u>Note</u>: This latter method is the basis for finite element methods