# UNIFIED LECTURE \#2: THE BREGUET RANGE EQUATION 

## I. Learning Goals

At the end of this lecture you will:
A. Be able to answer the question "How far can an airplane fly, and why?";
B. Be able to answer the question "How do the disciplines of structures \& materials, aerodynamics and propulsion jointly set the performance of aircraft, and what are the important performance parameters?";
C. Be able to use empirical evidence to estimate the performance of aircraft and thus begin to develop intuition regarding important aerodynamic, structural and propulsion system performance parameters;
D. Have had your first exposure to active learning in Unified Engineering

## II. Question: How far can an airplane (or a duck, for that matter) fly?



OR:

What is the farthest that an airplane can fly on earth, and why?

We will begin by developing a mathematical model of the physical system. Like most models, this one will have many approximations and assumptions that underlie it. It is important for you to understand these approximations and assumptions so that you understand the limits of applicability of the model and the estimates derived from it.


Figure 1.1 Force balance for an aircraft in steady level flight.

For steady, level flight,

$$
\mathrm{T}=\mathrm{D}, \quad \mathrm{~L}=\mathrm{W} \quad \text { or } \quad \mathrm{W}=\mathrm{L}=\mathrm{D} \frac{\mathrm{~L}}{\mathrm{D}}=\mathrm{T}\left(\frac{\mathrm{~L}}{\mathrm{D}}\right)
$$

The weight of the aircraft changes in response to the fuel that is burned (rate at which weight changes equals negative fuel mass flow rate times gravitational constant)

$$
\frac{\mathrm{dW}}{\mathrm{dt}}=-\dot{\mathrm{m}}_{\mathrm{f}} \cdot \mathrm{~g}
$$

Now we will define an overall propulsion system efficiency:

$$
\begin{align*}
& \text { overall efficiency }=\frac{\text { what you get }}{\text { what you pay for }}=\frac{\text { propulsive power }}{\text { fuel power }} \\
& \text { propulsive power }=\text { thrust } \cdot \text { flight velocity }=\mathrm{Tu}_{\mathrm{o}} \quad(\mathrm{~J} / \mathrm{s}) \\
& \text { fuel power }=\text { fuel mass flow rate } \cdot \text { fuel energy per unit mass }=\dot{\mathrm{m}}_{\mathrm{f}} \mathrm{~h} \tag{J/s}
\end{align*}
$$

Thus

$$
\eta_{\text {overall }}=\begin{gathered}
\mathrm{Tu}_{\mathrm{o}} \\
\dot{\mathrm{~m}}_{\mathrm{f}} \mathrm{~h}
\end{gathered}
$$

We can now write the expression for the change in weight of the vehicle in terms of important aerodynamic (L/D) and propulsion system ( $\eta_{\text {overall }}$ ) parameters:

$$
\frac{\mathrm{dW}}{\mathrm{dt}}=-\dot{\mathrm{m}}_{\mathrm{f}} \cdot \mathrm{~g}=\frac{-\mathrm{W}}{\left(\frac{\mathrm{~L}}{\mathrm{D}}\right) \frac{\mathrm{T}}{\dot{\mathrm{~m}}_{\mathrm{f}} \cdot \mathrm{~g}}}=\frac{-\mathrm{Wu}_{0}}{\frac{\mathrm{~h}}{\mathrm{~g}}\left(\frac{\mathrm{~L}}{\mathrm{D}}\right) \frac{\mathrm{Tu}_{0}}{\dot{\mathrm{~m}}_{\mathrm{f}} \cdot \mathrm{~h}}}=\frac{-\mathrm{Wu}_{0}}{\frac{\mathrm{~h}}{\mathrm{~g}}\left(\frac{\mathrm{~L}}{\mathrm{D}}\right) \eta_{\text {overall }}}
$$

We can rewrite and integrate

$$
\mathrm{dW}=\frac{-u_{0} \mathrm{dt}}{\frac{\mathrm{~h}}{\mathrm{~g}}\left(\frac{\mathrm{~L}}{\mathrm{D}}\right) \eta_{\text {overall }}} \quad \Rightarrow \quad \ln \mathrm{W}=\text { constant }-\frac{\mathrm{tu}_{0}}{\frac{\mathrm{~h}}{\mathrm{~g}}\left(\frac{L}{\mathrm{D}}\right) \eta_{\text {overall }}}
$$

applying the initial conditions, at $\mathrm{t}=0 \quad \mathrm{~W}=\mathrm{W}_{\text {initial }} \quad \therefore$ const. $=\ln \mathrm{W}_{\text {initial }}$

$$
\therefore \mathrm{t}={ }_{\mathrm{D}}^{-\mathrm{L}} \eta_{\text {overall }} \mathrm{gu}_{0} \mathrm{ln} \underset{W_{\text {initial }}}{\mathrm{W}}
$$

the time the aircraft has flown corresponds to the amount of fuel burned, therefore

$$
\mathrm{t}_{\text {final }}=\frac{-\mathrm{L}}{\mathrm{D}} \eta_{\text {overall }} \frac{\mathrm{h}}{\mathrm{gu}_{0}} \ln \frac{\mathrm{~W}_{\text {final }}}{\mathrm{W}_{\text {initial }}}
$$

then multiplying by the flight velocity we arrive at the Breguet Range Equation which applies for situations where overall efficiency, L/D, and flight velocity are constant over the flight.


Note that this expression is sometimes rewritten in terms of an alternate measure of efficiency, the specific fuel consumption or SFC. SFC is defined as the mass flow rate of fuel per unit of thrust ( $\mathrm{lbm} / \mathrm{s} / \mathrm{lbf}$ or $\mathrm{kg} / \mathrm{s} / \mathrm{N}$ ). In the following expression, V is the flight velocity and $g$ is the acceleration of gravity.

$$
\text { Range }=\frac{\mathrm{V}(\mathrm{~L} / \mathrm{D})}{\mathrm{g} \cdot \mathrm{SFC}} \ln \binom{\mathrm{~W}_{\text {initial }}}{\mathrm{W}_{\text {final }}}
$$

Thus we see that the answer to the question "How far can an airplane fly?" depends on:

1. How much energy is contained in the fuel it carries;
2. How aerodynamically efficient it is (the ratio of the production of lift to the production of drag). During the fluids lectures you will learn how to develop and use models to estimate lift and drag.
3. How efficiently energy from the fuel/oxidizer is turned into useful work (thrust times distance traveled) which is used to oppose the drag force. Thermodynamics helps us describe and estimate the efficiency of various energy conversion processes, and propulsion lets us describe how to use this energy to propel a vehicle;
4. How light weight the structure is relative to the amount of fuel and payload it can carry. The materials and structures lectures you will teach you how to estimate the performance of aerospace structures.

Below are some data to allow you to make estimates for various aircraft and birds.

|  | $\mathrm{MJ} / \mathrm{Kg}$ | \$/Kg | \$/MJ | Comments |
| :---: | :---: | :---: | :---: | :---: |
| Prime Beef | 4.0 | 20 | 5 |  |
| Beef | 4.0 | 8 | 2 |  |
| Whole Milk | 2.8 | 0.90 | 0.32 | $600 \mathrm{cal} /$ quart |
| Honey | 14 | 4 | 0.29 |  |
| Sugar | 15 | 1 | 0.07 | $100 \mathrm{cal} /$ ounce |
| Cheese | 15 | 6 | 0.40 |  |
| Bacon | 29 | 4 | 0.14 |  |
| Corn Flakes | 15 | 3.50 | 0.23 | $100 \mathrm{cal} /$ ounce |
| Peanut Butter | 27 | 4 | 0.15 | $180 \mathrm{cal} /$ ounce |
| Butter | 32 | 4.50 | 0.14 |  |
| Vegetable Oil | 36 | 2 | 0.06 | $240 \mathrm{cal} /$ ounce |
| Kerosene | 42 | 0.40 | 0.010 | $0.82 \mathrm{~kg} / \mathrm{liter}$ |
| Diesel Oil | 42 | 0.40 | 0.010 | $0.85 \mathrm{~kg} / \mathrm{liter}$ |
| Gasoline | 42 | 0.40 | 0.010 | $0.75 \mathrm{~kg} / \mathrm{liter}$ |
| Natural Gas | 45 | 0.24 | 0.005 | $0.8 \mathrm{~kg} / \mathrm{m}^{3}$ |

Figure 1.2 Heating values for various fuels (from The Simple Science of Flight, by H. Tennekes)


The Great Gliding Diagram. Airspeed, $V$, is plotted on the horizontal axis. Rate of descent, $w$, is plotted downward along the vertical axis. The diagonals are lines of constant finesse. The horizontal line represents the practical soaring limit, 1 meter / second.

Figure 1.3 Gliding performance as a function of $L / D$ (where $L / D=F$, from The Simple Science of Flight, by H. Tennekes)


Figure 1.4 Aerodynamic data for commercial aircraft: L/D for cruise (Babikian, R., The Historical Fuel Efficiency Characteristics of Regional Aircraft From Technological, Operational, and Cost Perspectives, SM Thesis, MIT, June 2001)

|  | W <br> (N) | $\begin{aligned} & S \\ & \left(\mathrm{~m}^{2}\right) \end{aligned}$ | b <br> (m) | A | $F$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| House Sparrow | 0.28 | 0.009 | 0.23 | 6 | 4 |
| Swift | 0.36 | 0.016 | 0.42 | 11 | 10 |
| Common Tern | 1.2 | 0.056 | 0.83 | 12 | 12 |
| Kestrel (Sparrow Hawk) | 1.8 | 0.06 | 0.74 | 9 | 9 |
| Carrion Crow | 5.5 | 0.12 | 0.78 | 5 | 5 |
| Common Buzzard | 8.0 | 0.22 | 1.25 | 7 | 10 |
| Peregrine Falcon | 8.1 | 0.13 | 1.06 | 9 | 10 |
| Herring Gull | 12 | 0.21 | 1.43 | 10 | 11 |
| Heron | 14 | 0.36 | 1.73 | 8 | 9 |
| White Stork | 34 | 0.50 | 2.00 | 8 | 10 |
| Wandering Albatross | 85 | 0.62 | 3.40 | 19 | 20 |
| Hang Glider | 1000 | 15 | 10 | 7 | 8 |
| Parawing | 1000 | 25 | 8 | 2.6 | 4 |
| Powered Parawing | 1700 | 35 | 10 | 2.7 | 4 |
| Ultralight (microlight) | 2000 | 15 | 10 | 7 | 8 |
| Sailplanes |  |  |  |  |  |
| Standard Class | 3500 | 10.5 | 15 | 21 | 40 |
| Open Class | 5500 | 16.3 | 25 | 38 | 60 |
| Fokker F-50 | $19 \times 10^{4}$ | 70 | 29 | 12 | 16 |
| Boeing 747 | $36 \times 10^{5}$ | 511 | 60 | 7 | 15 |

Figure 1.5 Weight and geometry for aircraft and birds (where $\mathrm{L} / \mathrm{D}=\mathrm{F}$, from The Simple Science of Flight, by H. Tennekes)


Weight Fractions of Cargo and Passenger Aircraft

Figure 1.5 Weight fractions for transport aircraft in terms of empty weight over max take-off weight (Mattingly, Heiser \& Daley, Aircraft Engine Design, 1987)


Figure 1.6 Structural efficiency data for commercial aircraft: Operating empty weight over maximum take-off weight (Babikian, R., The Historical Fuel Efficiency Characteristics of Regional Aircraft From Technological, Operational, and Cost Perspectives, SM Thesis, MIT, June 2001)

|  | Takeoff weight $W$ (tons) | $S\left(\mathrm{~m}^{2}\right)$ | $b$ (m) | Sea-level thrust $T$ (tons) | Fuel consumption (liters/hour) | $\begin{gathered} \text { Cruising } \\ \text { speed } \\ V(\mathrm{~km} / \text { hour }) \end{gathered}$ | Range (km) | Seats |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Boeing 747-400 | 395 | 530 | 65 | $4 \times 25.7$ | 12300 | 900 | 12200 | 421 |
| Boeing 747-300 | 378 | 511 | 60 | $4 \times 23.8$ | 13600 | 900 | 10500 | 400 |
| Boeing $747-200$ | 352 | 511 | 60 | $4 \times 21.3$ | 13900 | 900 | 9500 | 387 |
| Douglas <br> Dc-10-30 | 256 | 368 | 50 | $3 \times 23.1$ | 10400 | 900 | 9900 | 248 |
| Airbus A310 | 139 | 219 | 44 | $2 \times 22.7$ | 5500 | 860 | 6400 | 200 |
| Boeing 737-300 | 57 | 105 | 29 | $2 \times 9.1$ | 2700 | 800 | 4200 | 124 |
| Fokker F-100 | 43 | 94 | 28 | $2 \times 6.7$ | 2400 | 720 | 1800 | 101 |
| Fokker <br> F-28 | 33 | 79 | 25 | $2 \times 4.5$ | 2500 | 680 | 1700 | 80 |

Figure 1.7 Aircraft performance (from The Simple Science of Flight, by H. Tennekes)
For aircraft engines it is often convenient to break the overall efficiency into two parts: thermal efficiency and propulsive efficiency where the subscripts e and o refer to exit and inlet:

$$
\begin{aligned}
& \eta_{\text {thermal }}=\frac{\text { rate of production of propellant k.e. }}{\text { fuel power }}=\frac{\left(\frac{\dot{\mathrm{m}}_{\mathrm{e}} \mathrm{u}_{\mathrm{e}}^{2}}{2}-\frac{\dot{\mathrm{m}}_{\mathrm{o}} \mathrm{u}_{\mathrm{o}}^{2}}{2}\right)}{\dot{\mathrm{m}}_{\mathrm{f}} \mathrm{~h}} \\
& \eta_{\text {prop }}=\begin{array}{c}
\text { rate of production of propellant k.e. }
\end{array}=\frac{\mathrm{Tu}_{\mathrm{o}}}{\left(\frac{\dot{\mathrm{~m}}_{\mathrm{e}} \mathrm{u}_{\mathrm{e}}^{2}}{2}-\frac{\dot{\mathrm{m}}_{\mathrm{o}} \mathrm{u}_{\mathrm{o}}^{2}}{2}\right)}
\end{aligned}
$$

such that

$$
\eta_{\text {overall }}=\eta_{\text {thermal }} \cdot \eta_{\text {prop }}
$$

During the first semester thermodynamics lectures we will focus largely on thermal efficiency. In next semester's propulsion lectures we will combine thermodynamics with fluid mechanics to obtain estimates for propulsive and thus overall efficiency. The data shown in Figure 1.6 will give you a rough idea for the conversion efficiencies of various modern aircraft engines.


Figure 1.8 Trends in aircraft engine efficiency (after Pratt \& Whitney)


Figure 1.9 Engine efficiency for commercial aircraft: specific fuel consumption (Babikian, R., The Historical Fuel Efficiency Characteristics of Regional Aircraft From Technological, Operational, and Cost Perspectives, SM Thesis, MIT, June 2001)

The accuracy of the range equation in predicting performance for commercial transport aircraft is quite good. The Department of Transportation collects and reports a variety of operational and financial data for the U.S. fleet in something called DOT Form 41. Operational data for fuel burned and payload (passengers and cargo) carried was extracted from Form 41 and combined with the technological data shown in Figures 1.4, 1.6 and 1.9 to estimate range. In Figure 1.10 these estimates are compared to the actual stage length flown (range) as reported in Form 41. The difference between the actual stage length flown and the estimated stage length is shown in Figure 1.11. Figure 1.11 shows that the percent deviation between the Breguet range equation estimates and the actual stage lengths flown is a function of the stage length. For long-haul flights, the assumptions of constant velocity, L/D, and SFC are good. However, for short-haul flights, taxiing, climbing, descending, etc. are a relatively large fraction of the overall flight time, so the steady-state cruise assumptions of the range equation are less valid.
(16 short- and long-haul aircraft)


Figure 1.10 Performance of Breguet range equation for estimating commercial aircraft operations (J. J. Lee, MIT Masters Thesis, 2000)


Figure 1.11 Deviation (\%) of Breguet range equation estimates from actual stage length flown is a function of the stage length (J. J. Lee, MIT Masters Thesis, 2000)

## III. Questions:

A. How far can a duck fly?
B. Why don't we fly on hydrogen-powered airplanes?

Fuel properties are listed below.

| Fuel | Density $\left(\mathrm{kg} / \mathrm{m}^{3}\right)$ | Heating Value $(\mathrm{kJ} / \mathrm{kg})$ |
| :--- | :--- | :--- |
| Jet-A | 800.0 | 45000 |
| $\mathrm{H}_{2}$ (gaseous, S.T.P.) | 0.0824 | 120900 |
| $\mathrm{H}_{2}$ (liquid, 1 atm$)$ | 70.8 | 120900 |

C. Why is the maximum range for an aircraft on earth approximately $25,000 \mathrm{mi}$ ? (Voyager: 3181 kg of fuel is $72 \%$ of maximum take-off weight, flight speed $186.1 \mathrm{~km} / \mathrm{hr}=9$ days to circle the earth)
D. What are the assumptions and approximations that underlie the Breguet Range Equation?

